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(54) **METHOD AND SYSTEM FOR TREATING ANEURYSMS**

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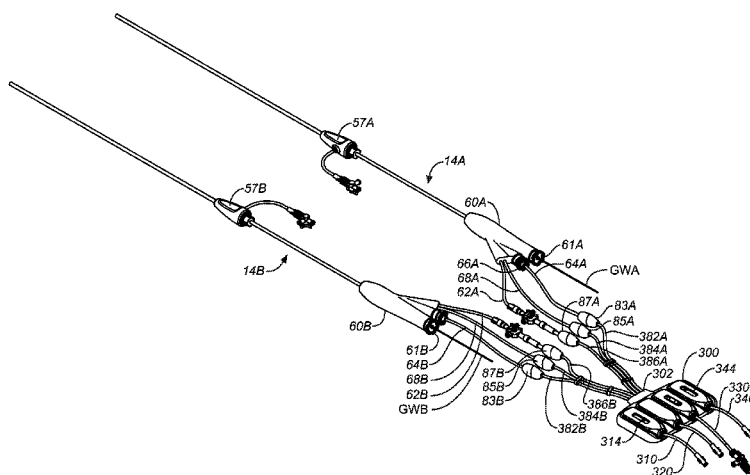
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ABSTRACT

Methods for treatment of aneurysms using a sequential manifold console to deploy multiple filling structures are provided herein. In one aspect, aneurysms are treated by simultaneously filling two double-walled filling structure using a sequential manifold console to guide a user in the steps to be followed in the procedure and to reliably achieve a consistent and durable aneurysmal treatment using a curable medium. The structures may be delivered over balloon deployment mechanisms in order to shape and open tubular lumens there-through. Pairs of filling structures delivered to the aneurysm from different access openings of a patient can be simultaneously prepared and pressurized from a single treatment console when treating abdominal aortic aneurysms using the described systems and methods.

8 Claims, 38 Drawing Sheets



US 9,415,195 B2

Page 2

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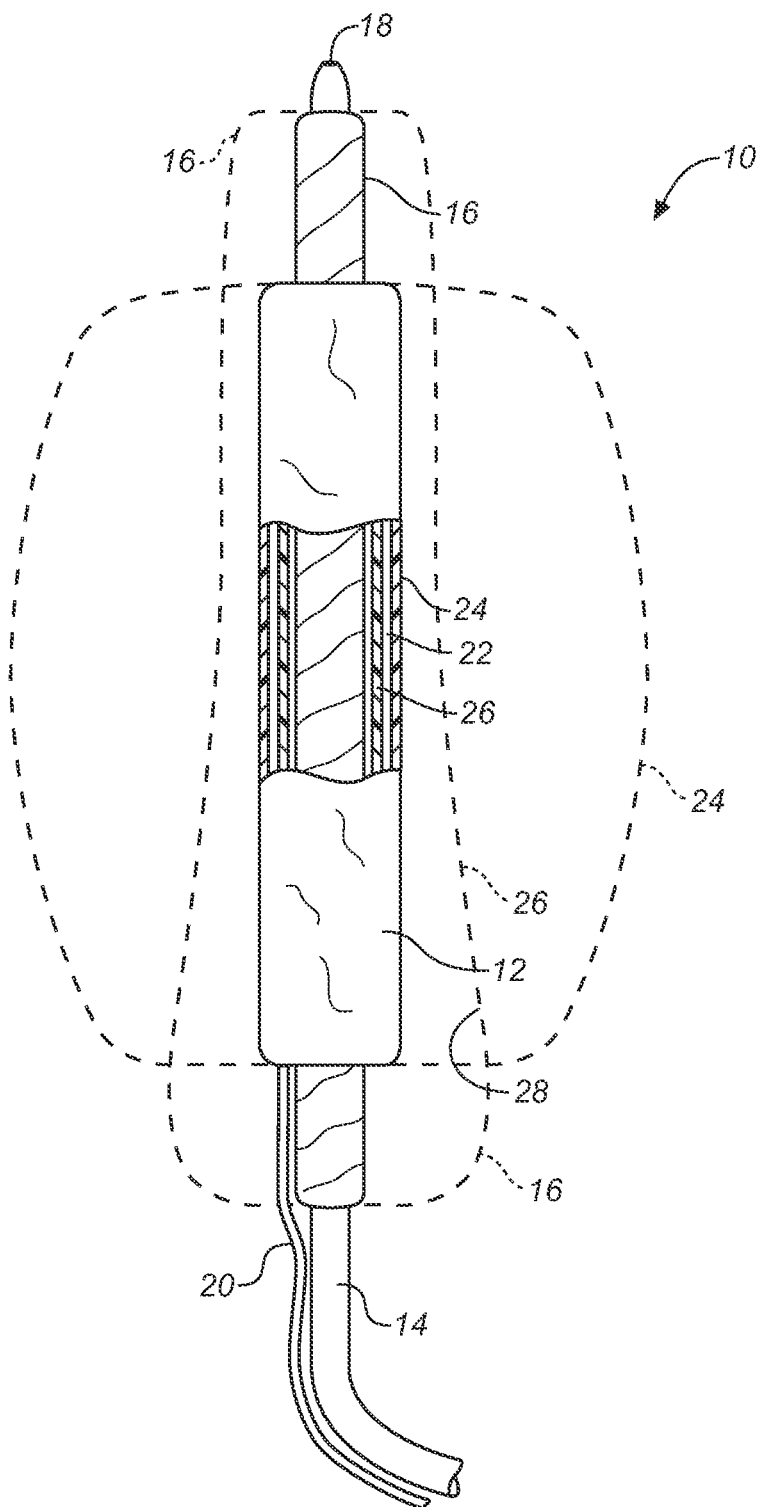


FIG. 1

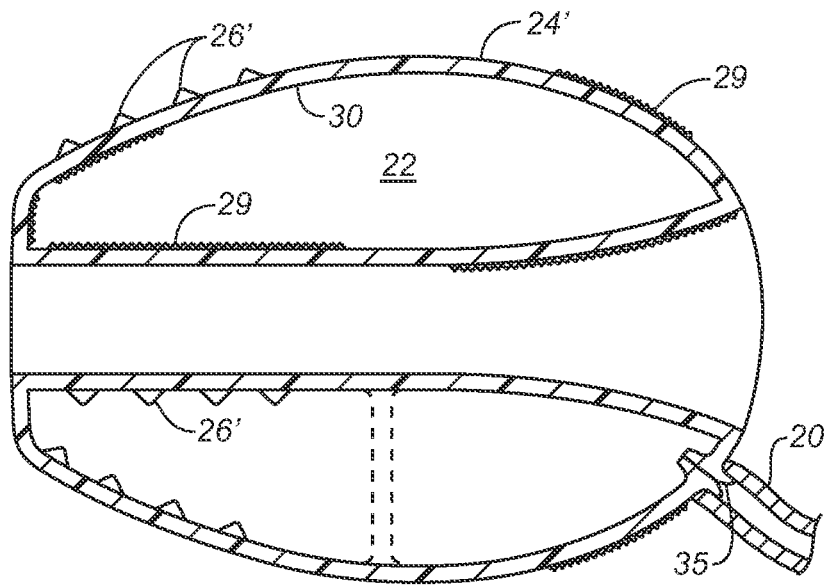


FIG. 2

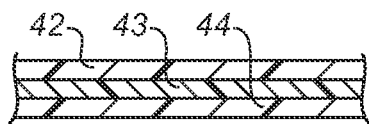


FIG. 3A

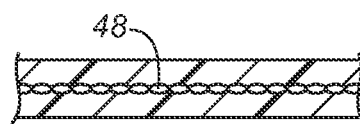


FIG. 3B

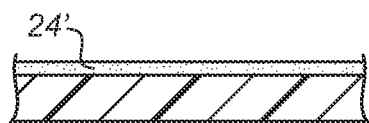


FIG. 3C

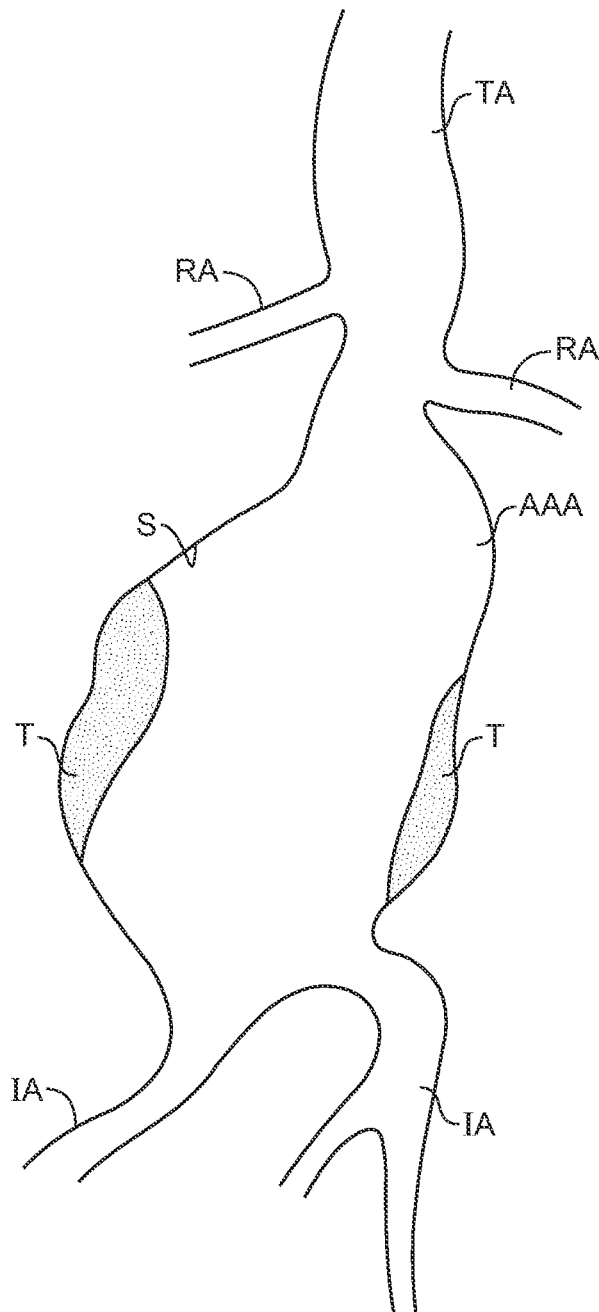


FIG. 4

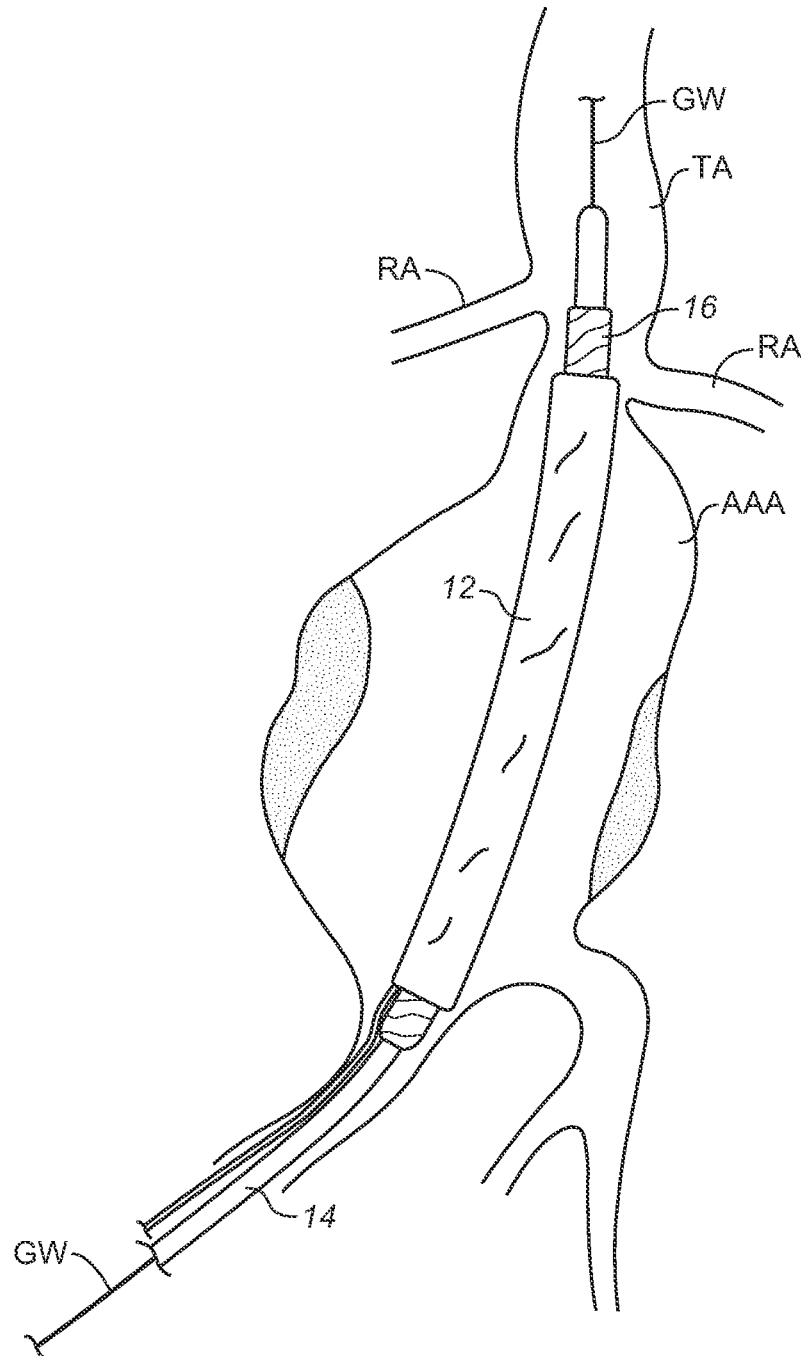


FIG. 5A

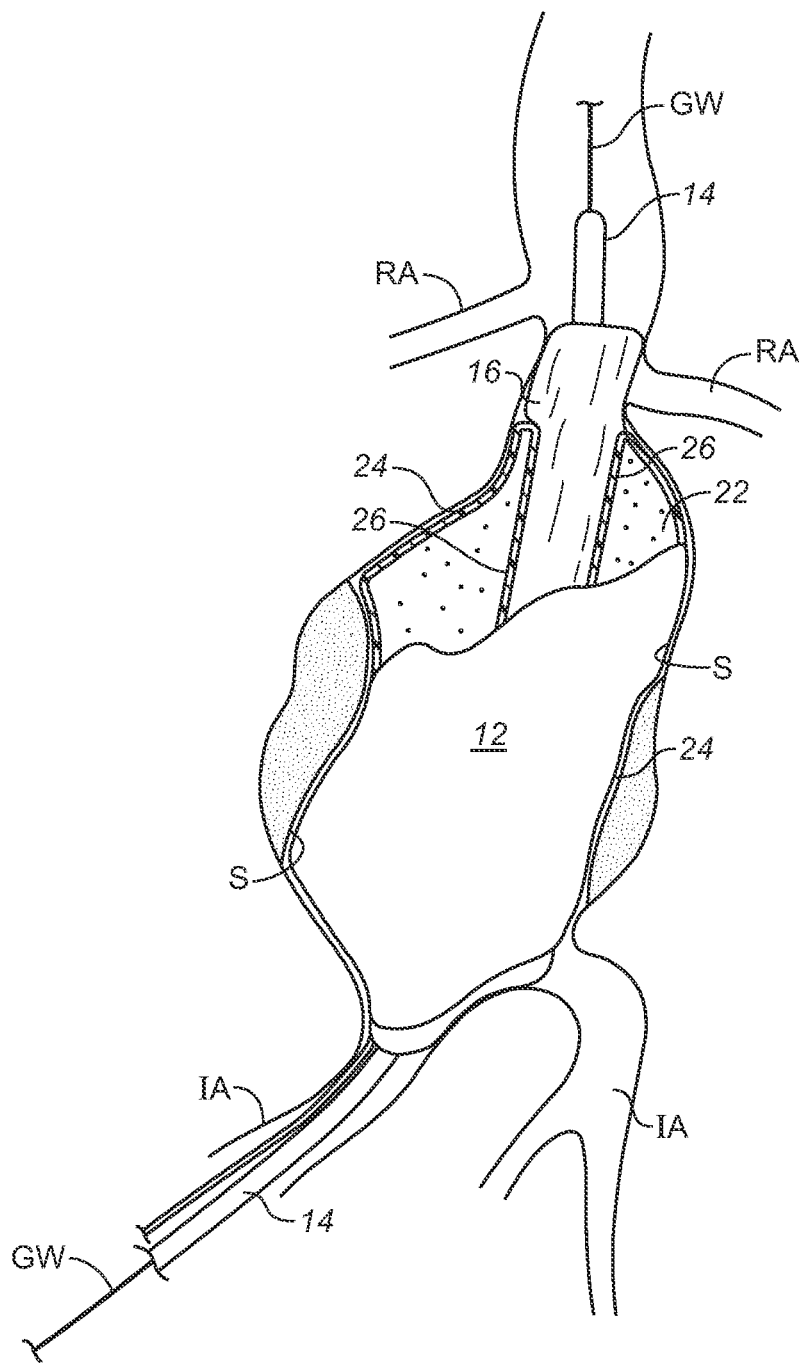


FIG. 5B

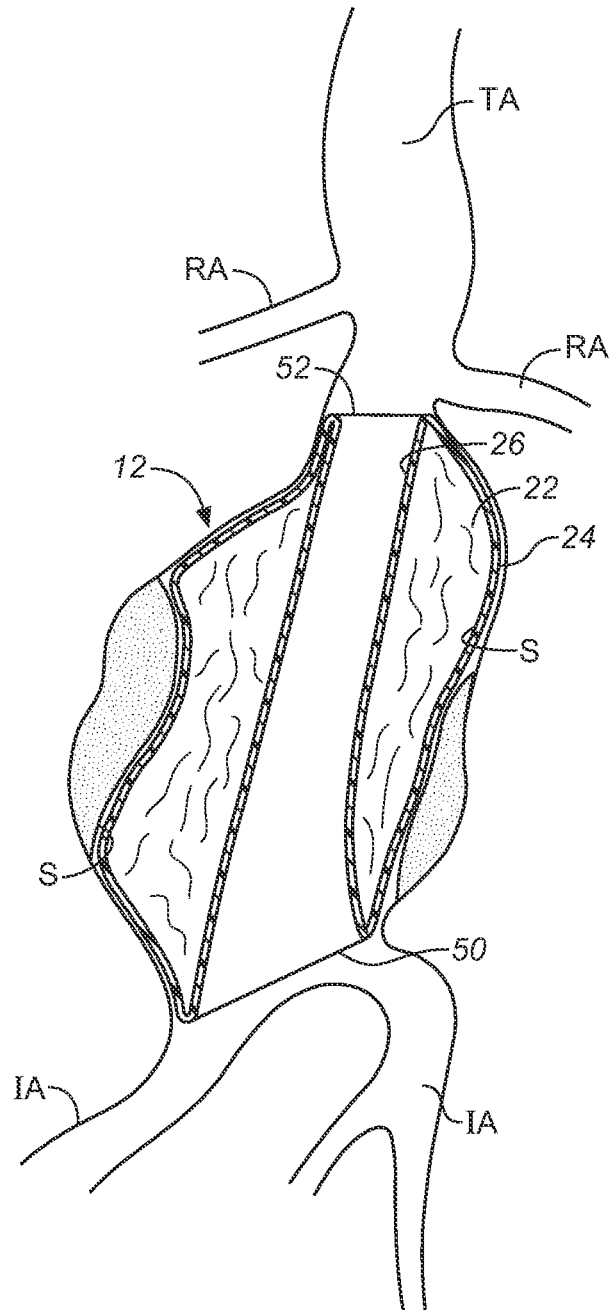


FIG. 5C

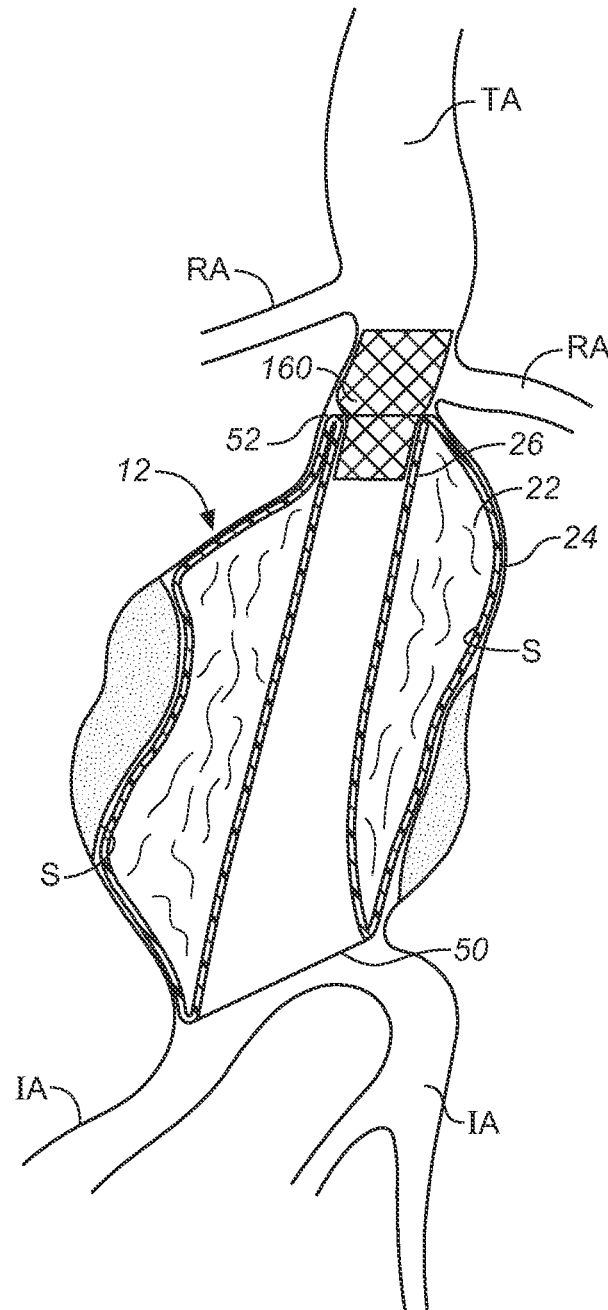


FIG. 5D

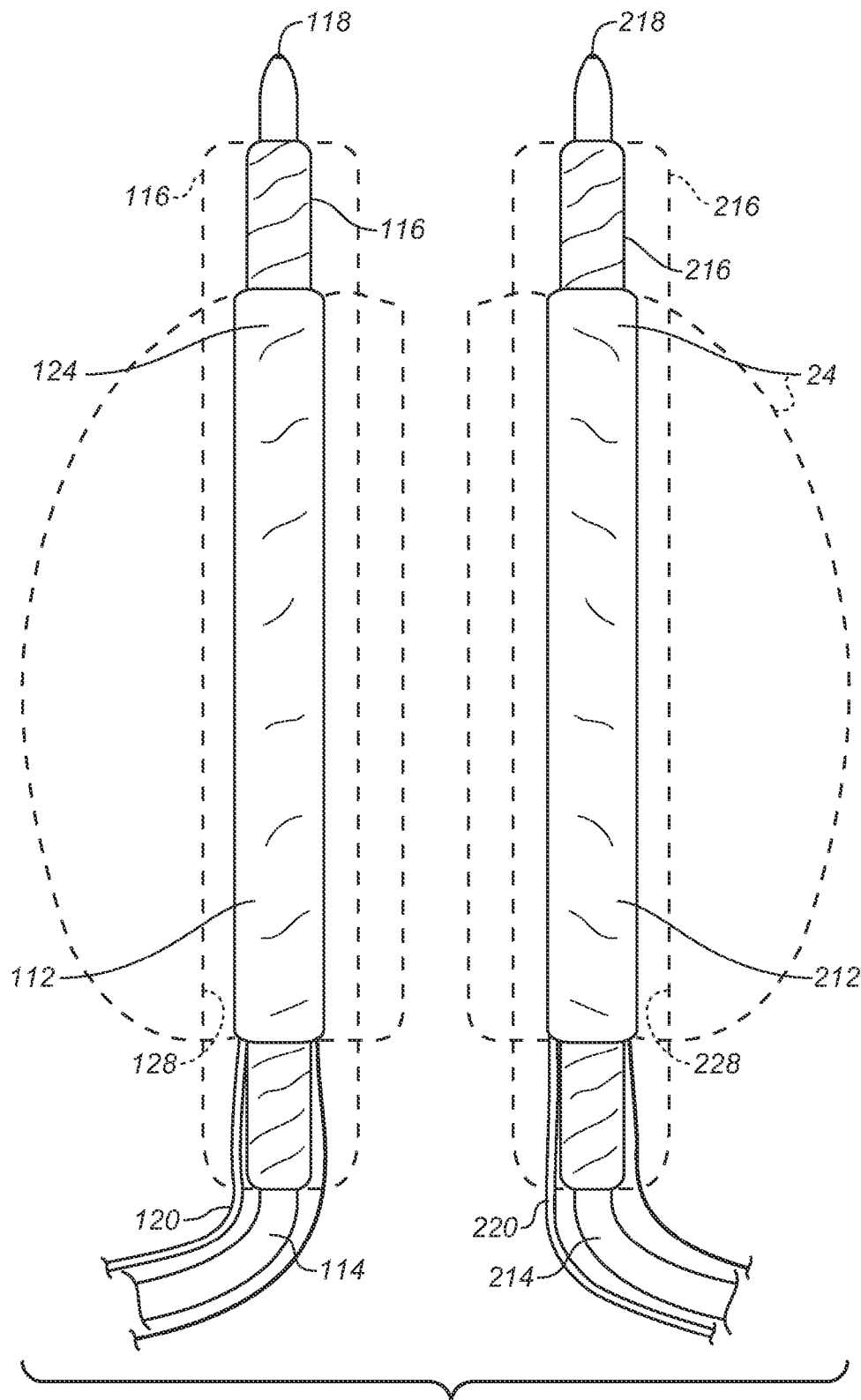


FIG. 6

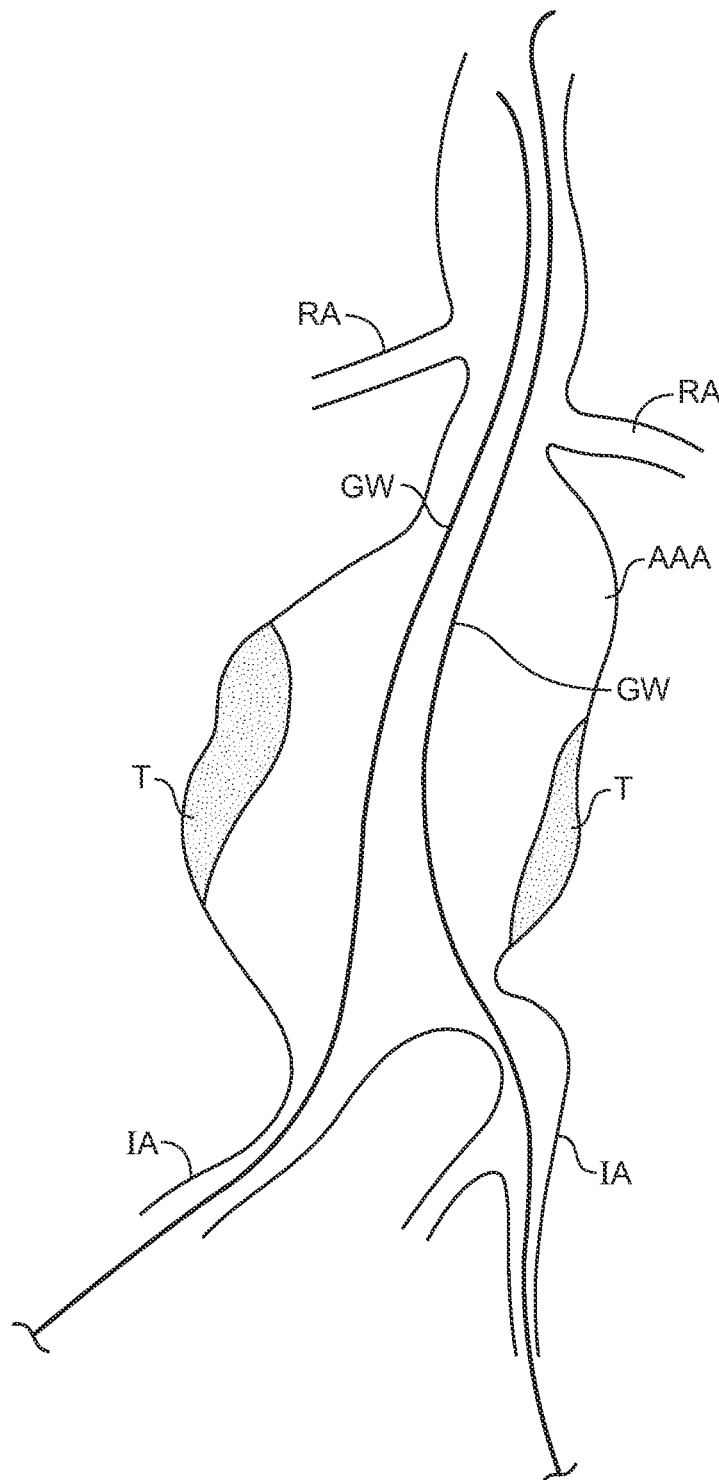


FIG. 7A

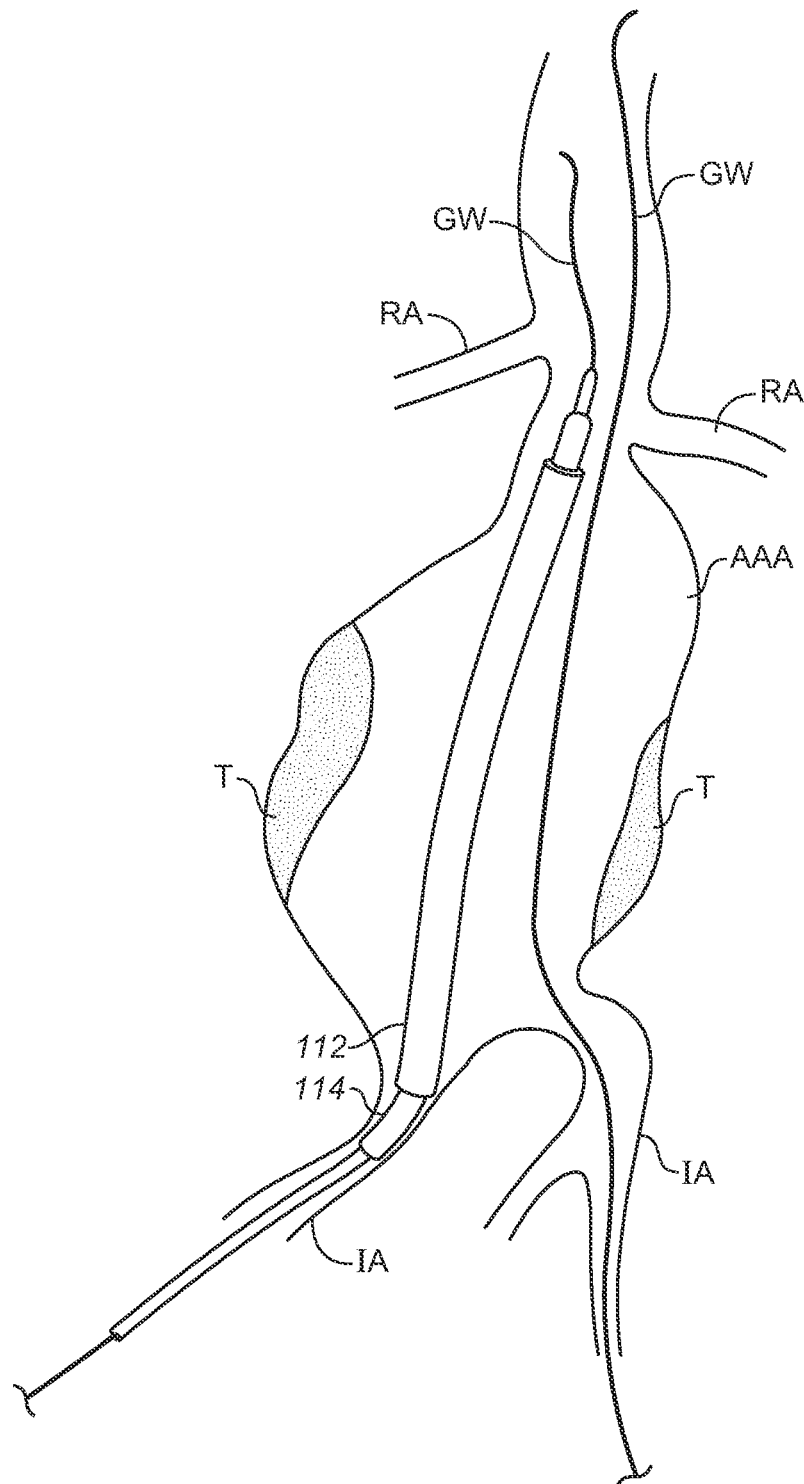


FIG. 7B

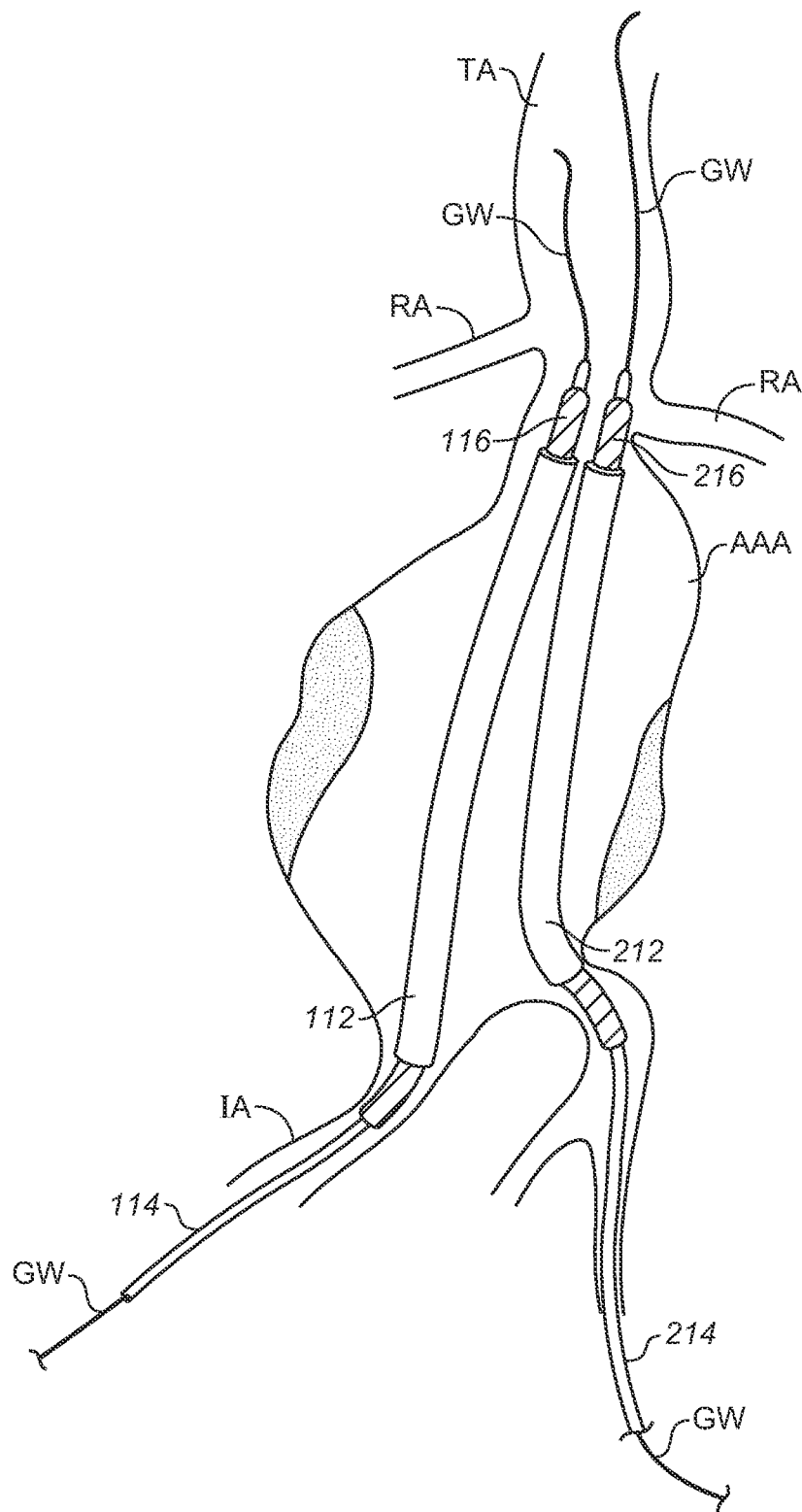


FIG. 7C

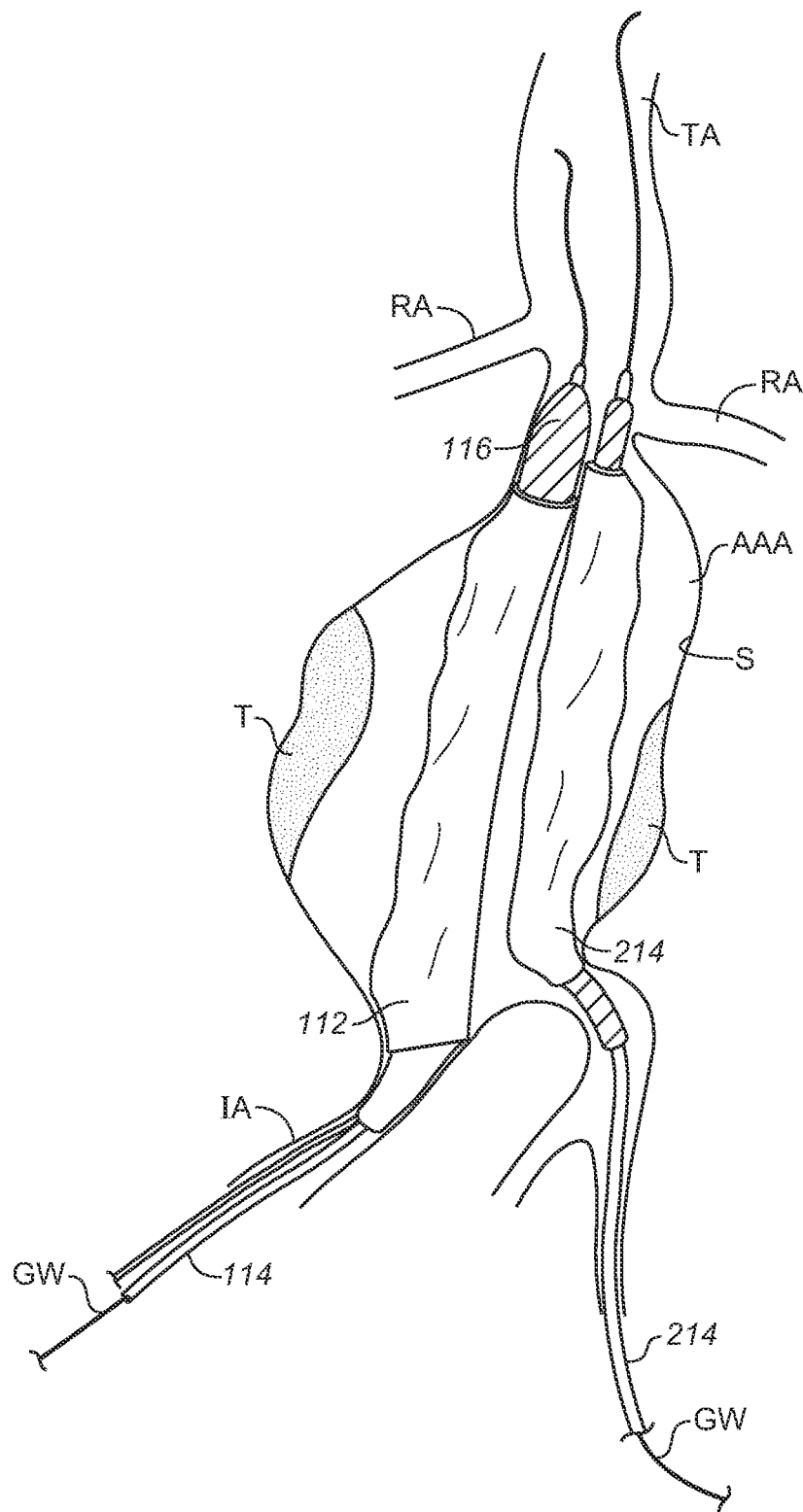


FIG. 7D

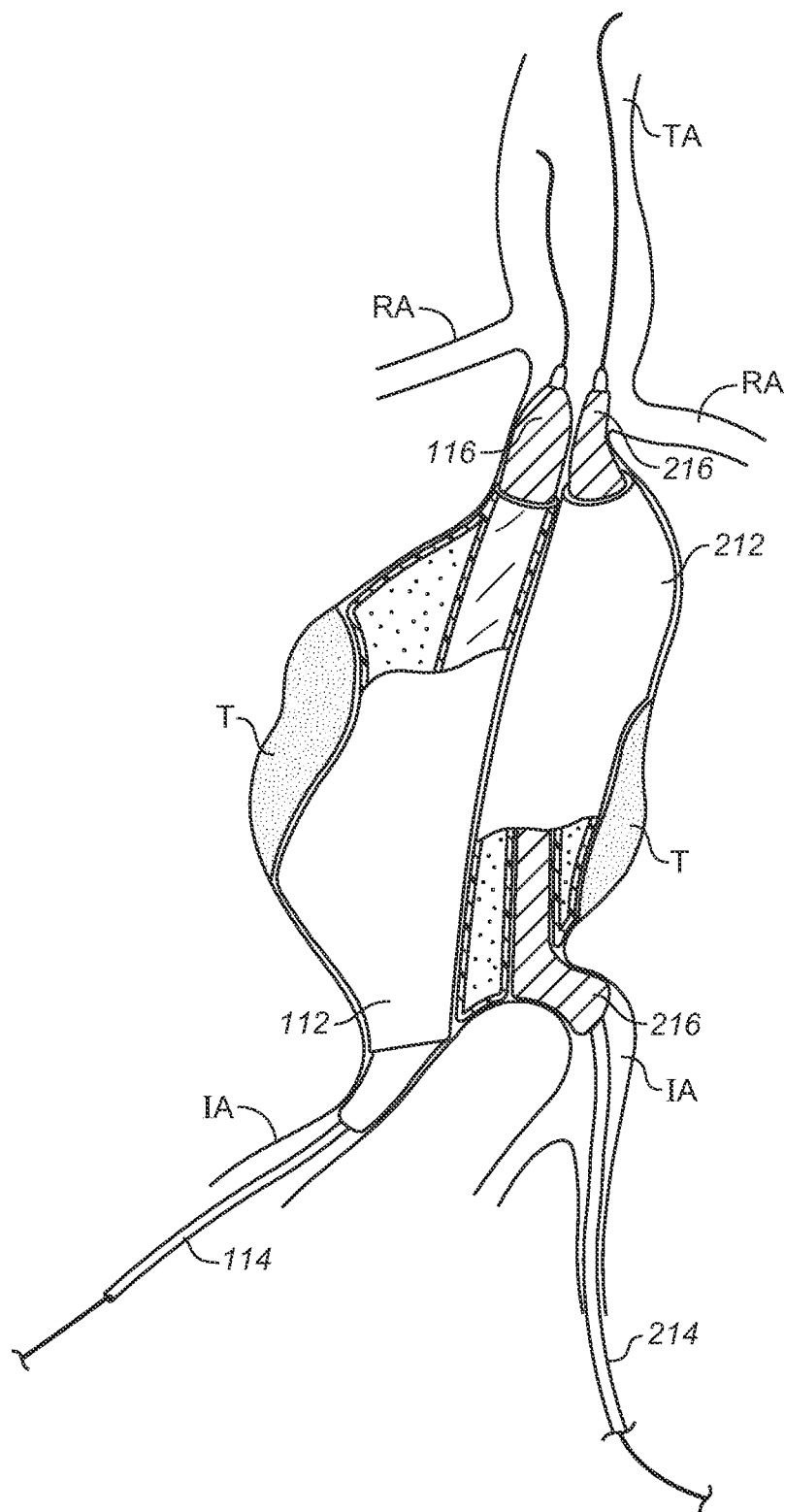


FIG. 7E

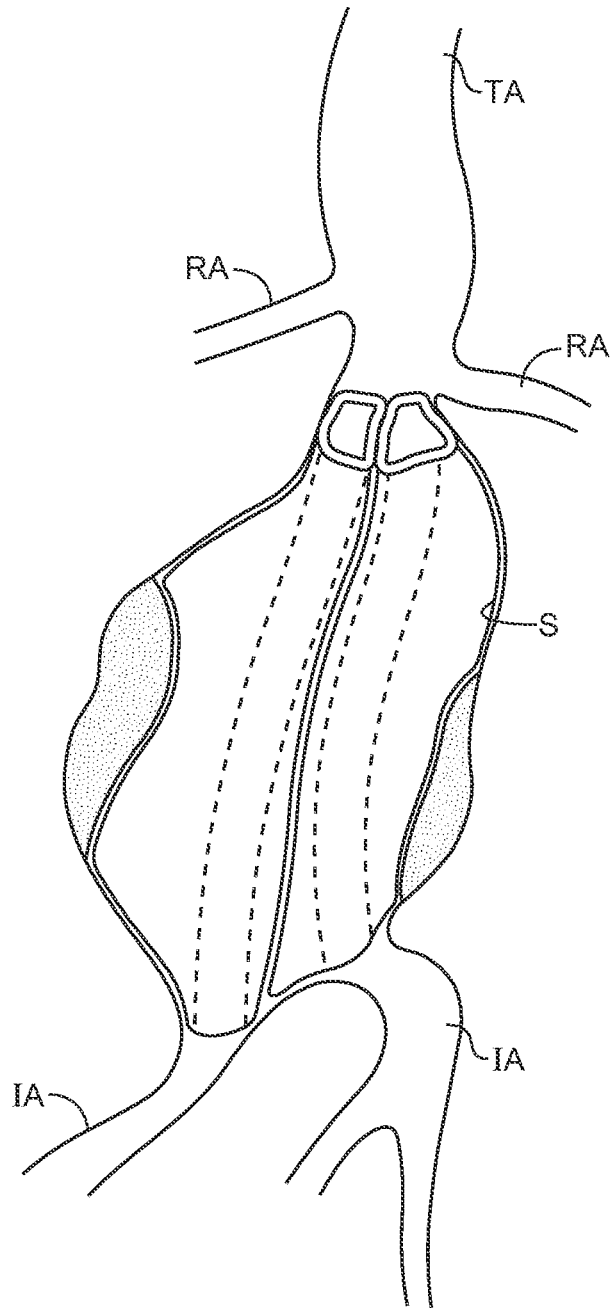


FIG. 7F

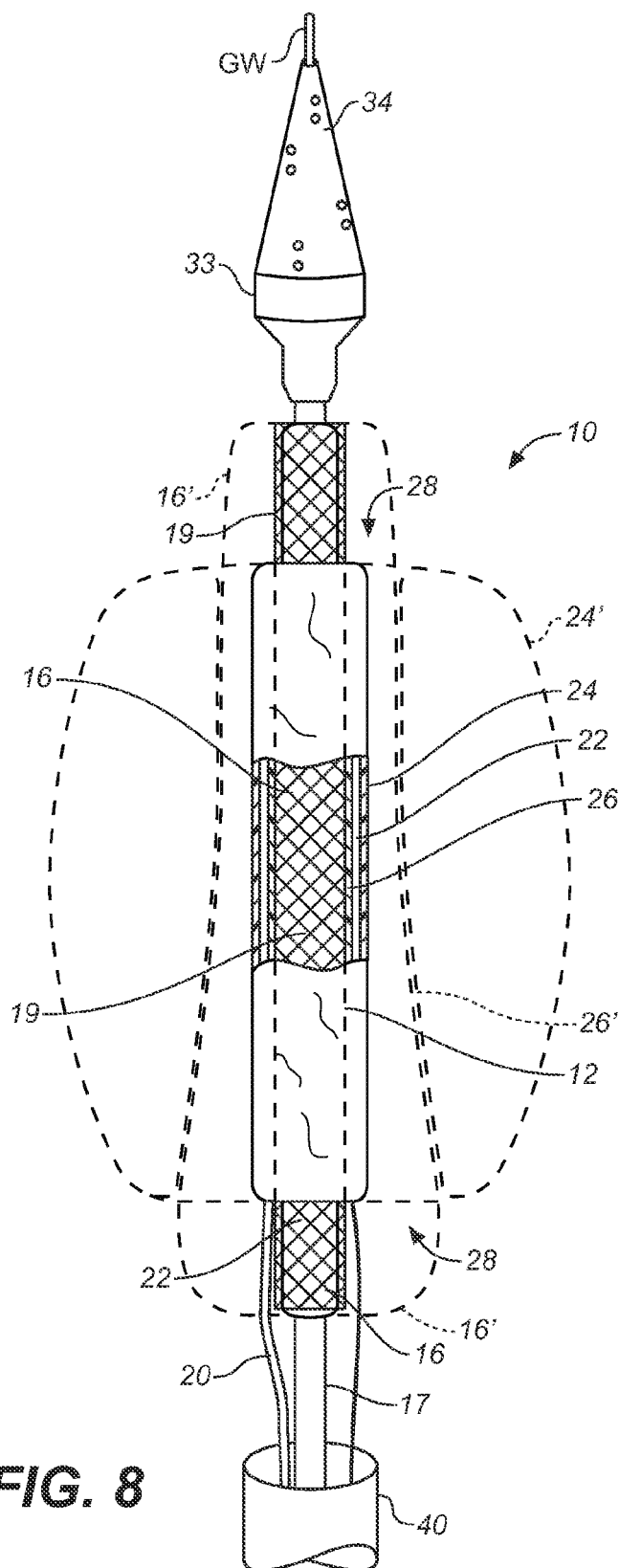


FIG. 8

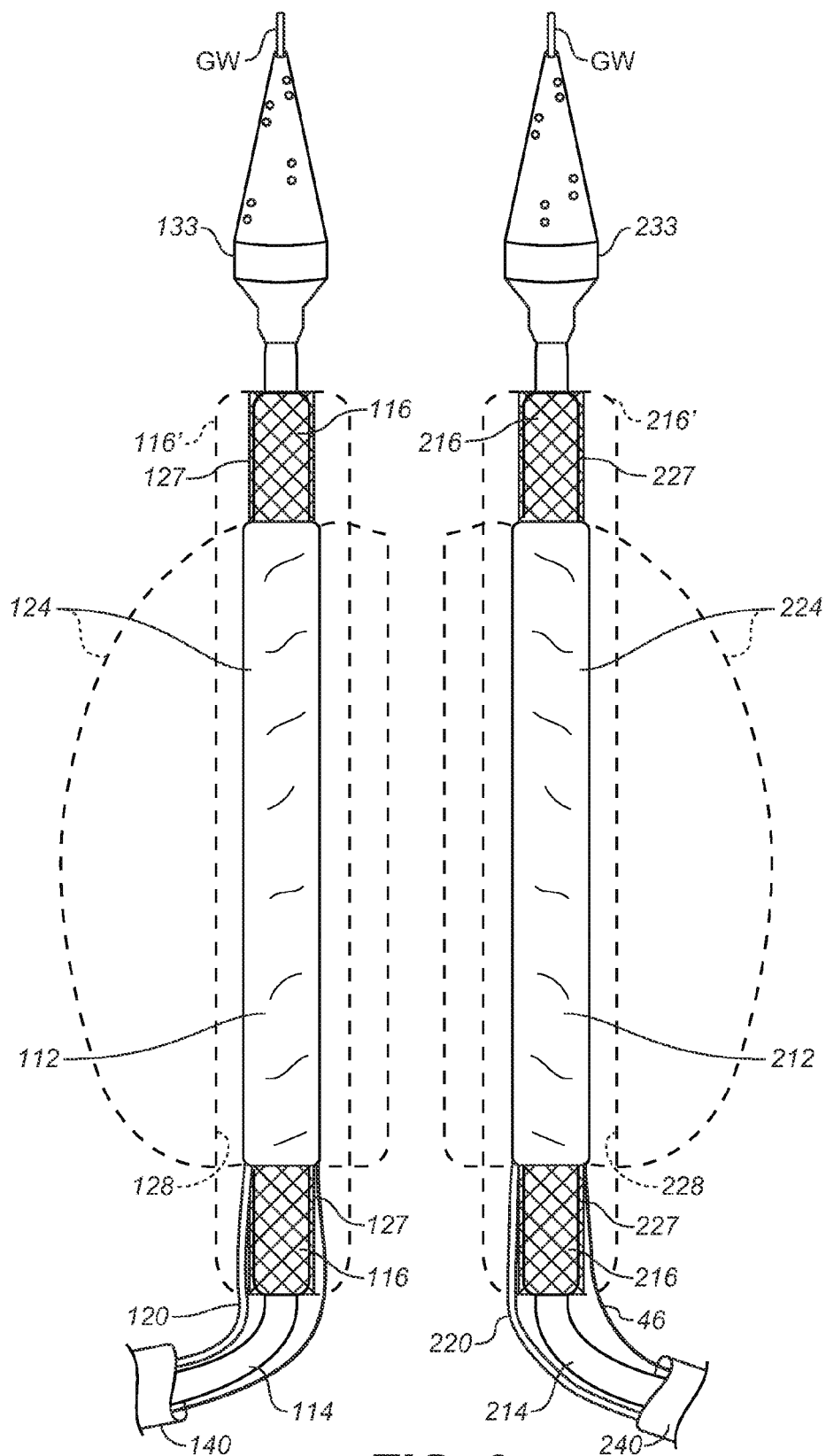
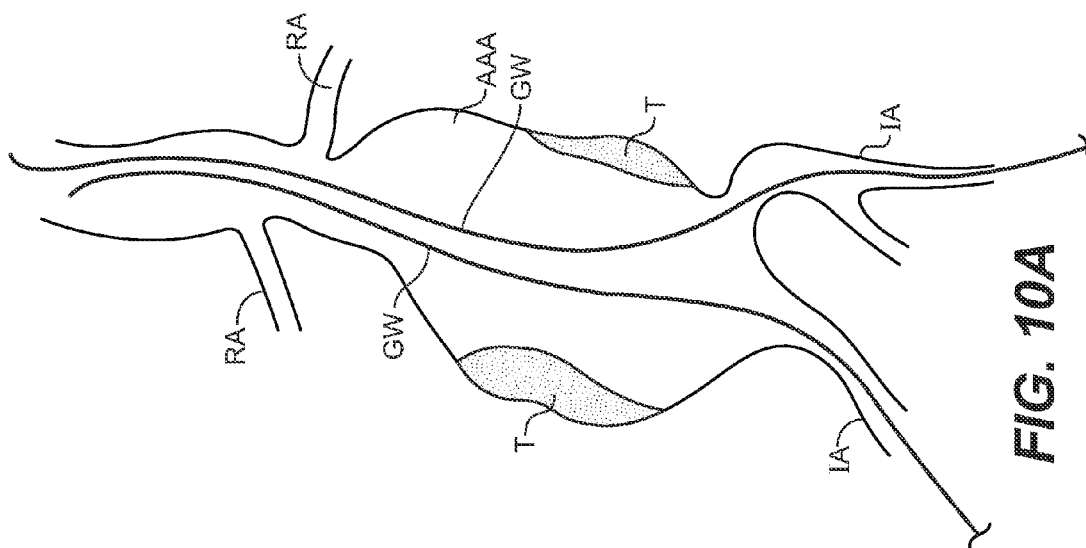
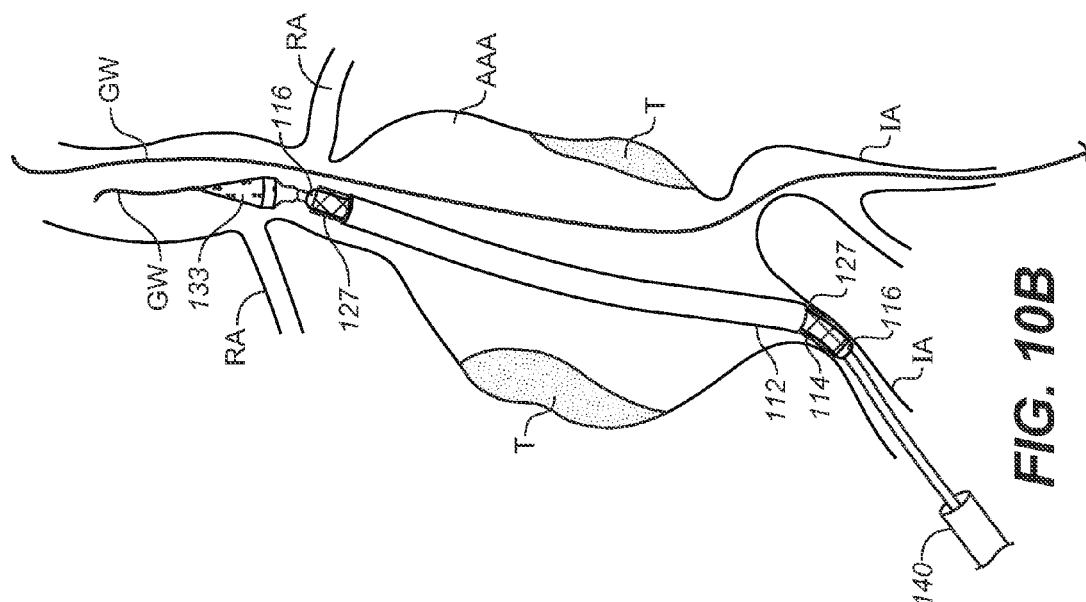


FIG. 9



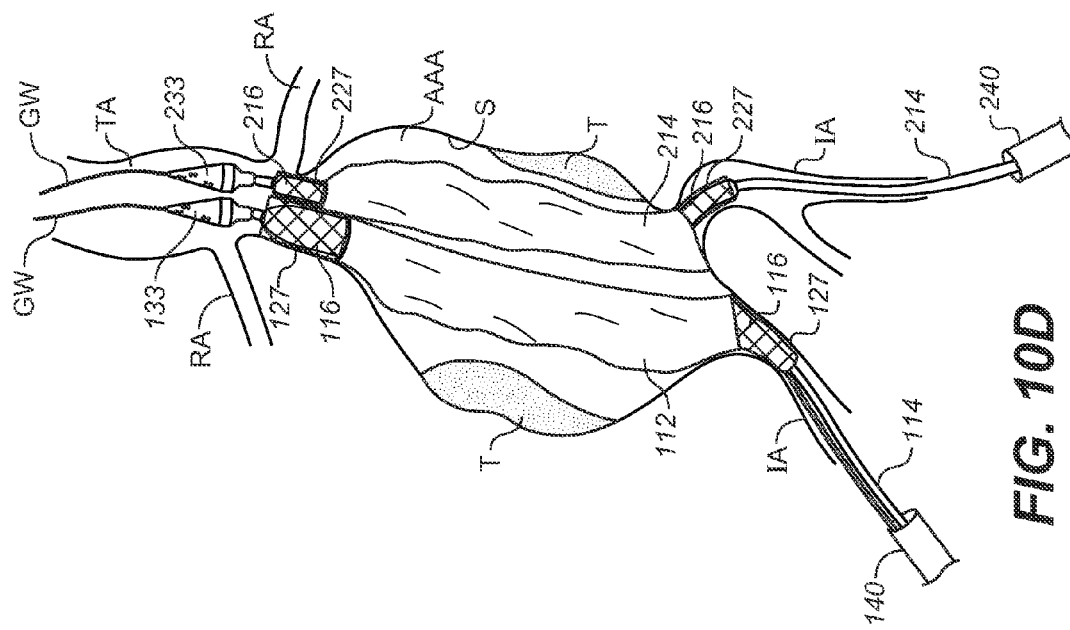


FIG. 10D

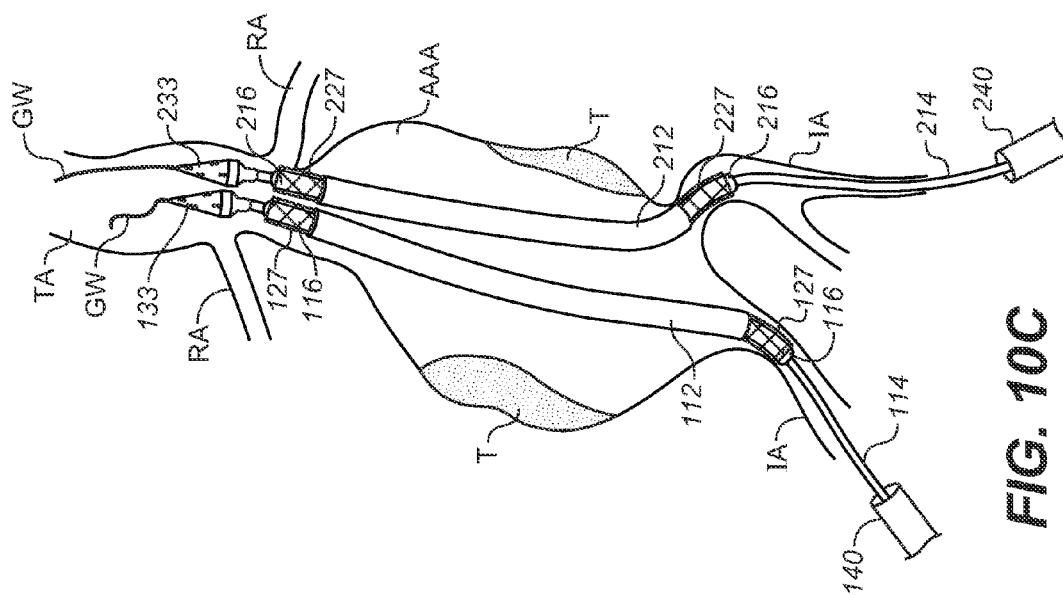


FIG. 10C

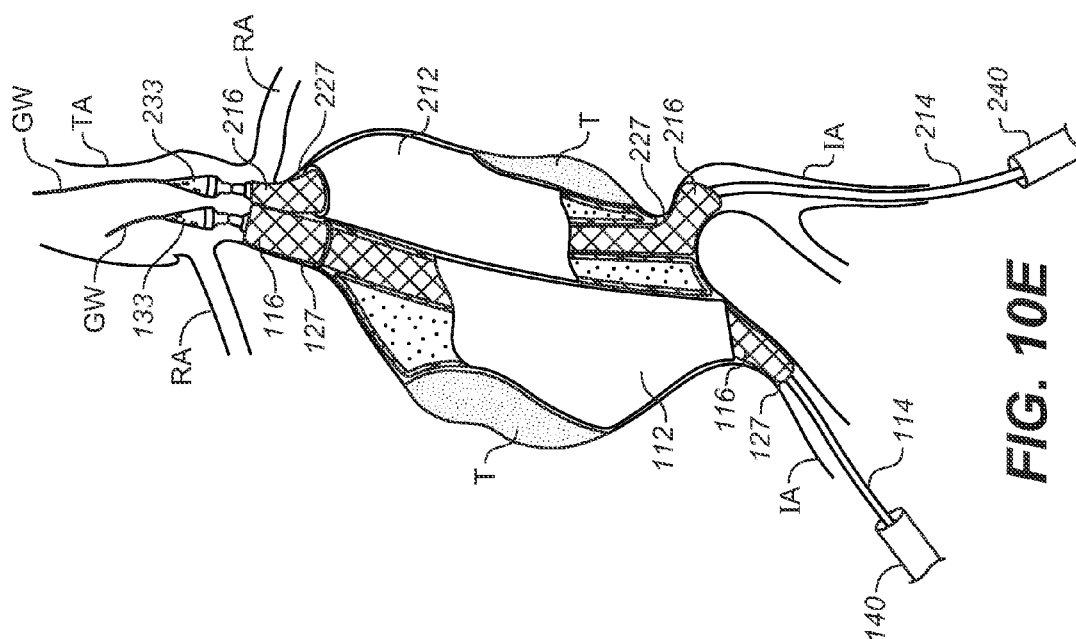


FIG. 10E

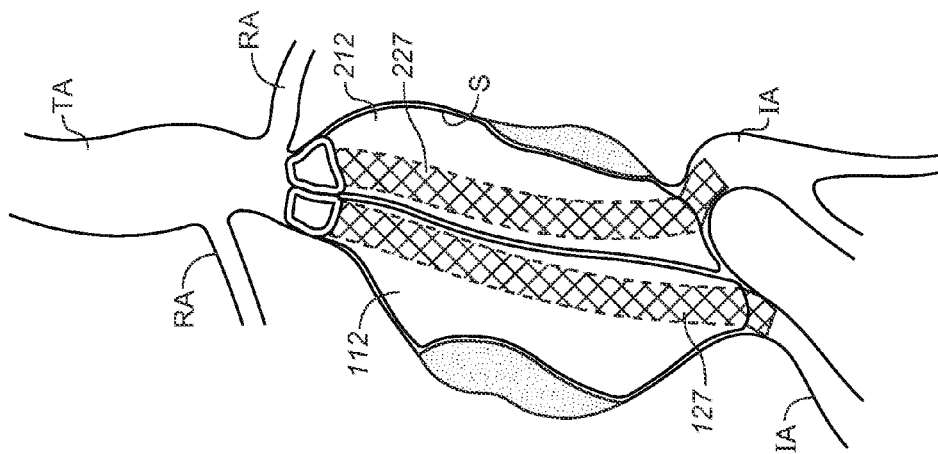


FIG. 10F

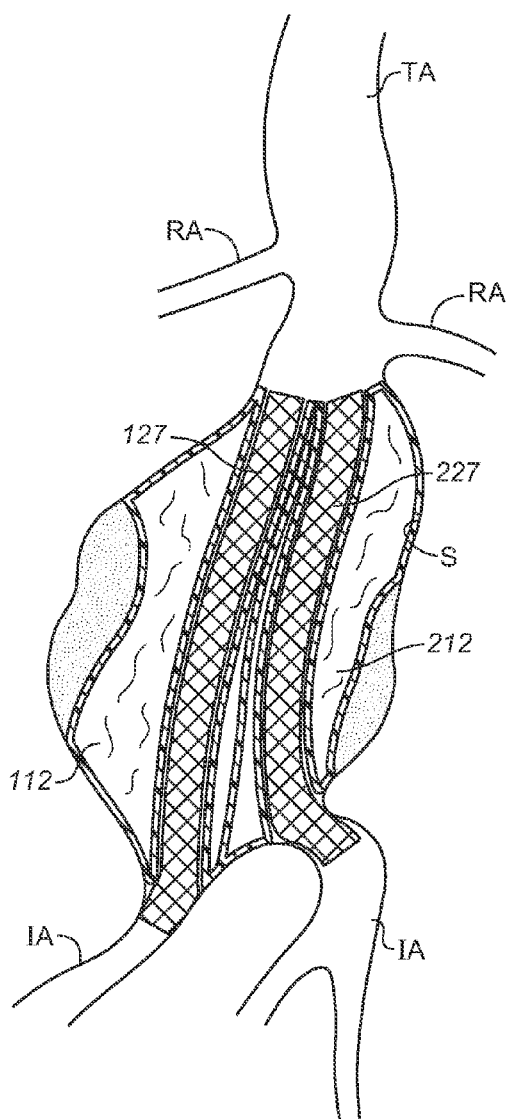


FIG. 10G

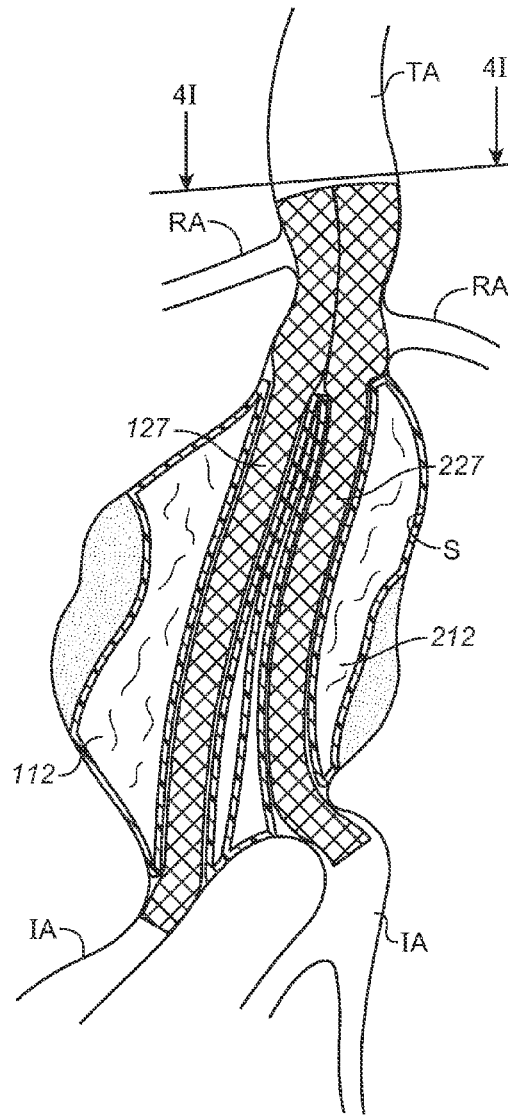


FIG. 10H

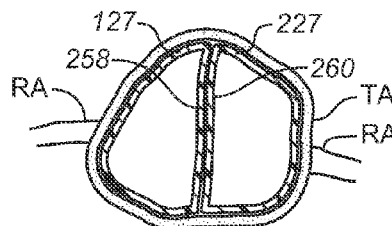
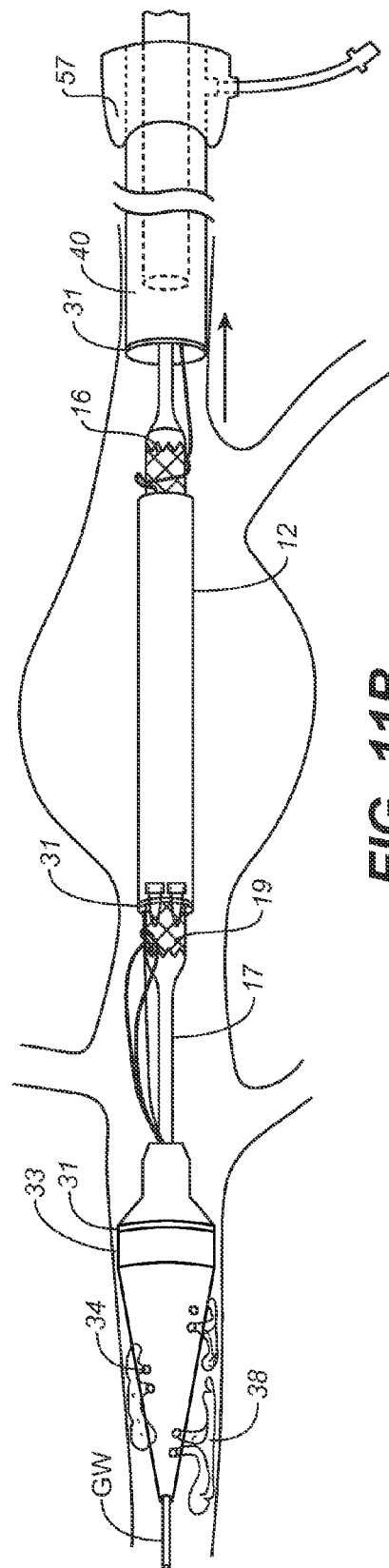
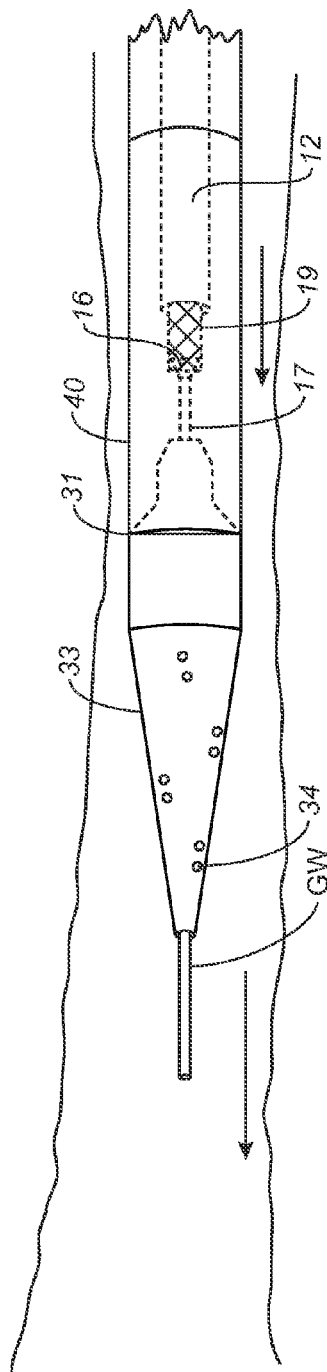
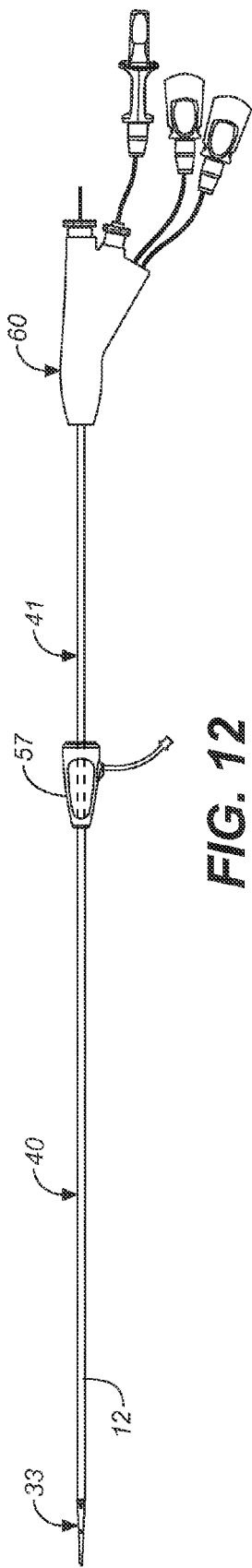


FIG. 10I





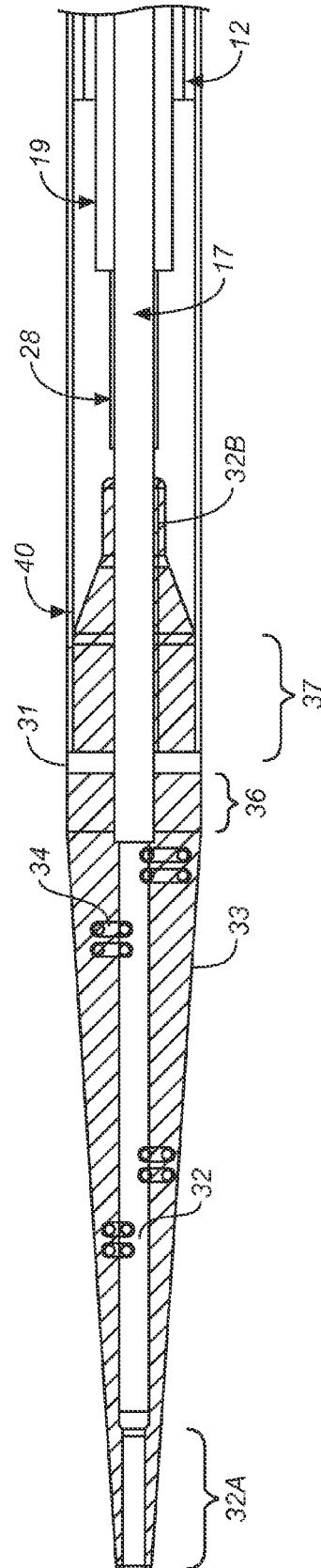


FIG. 13

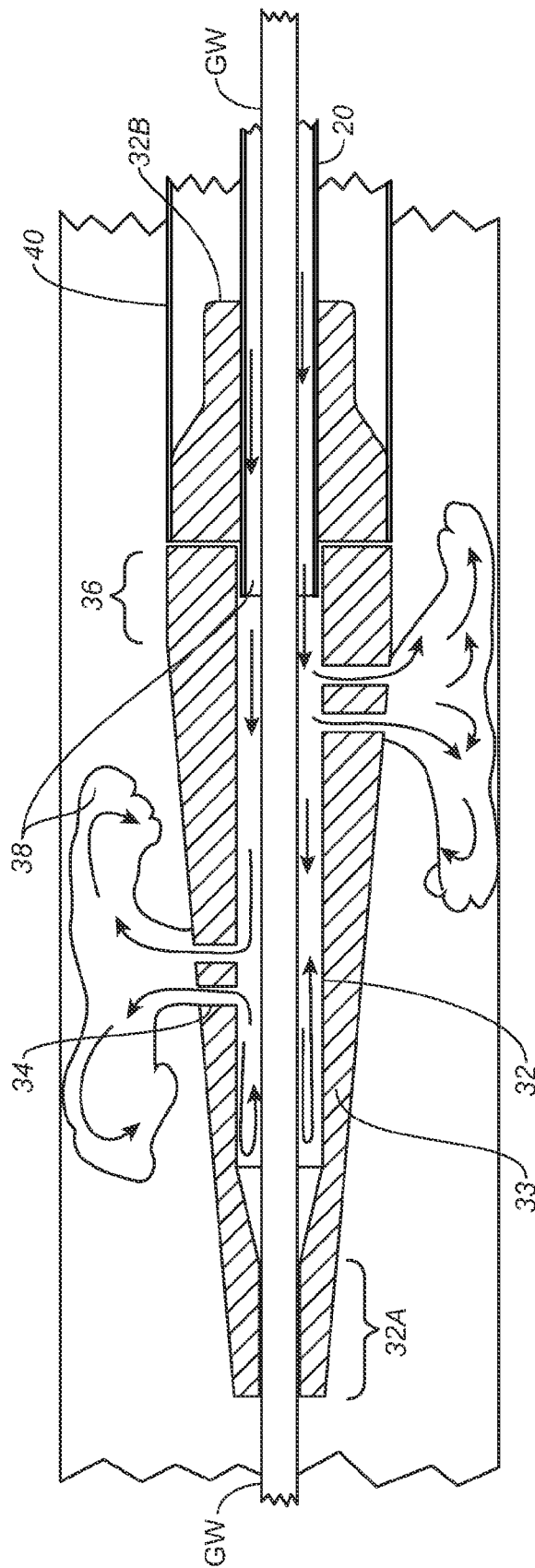
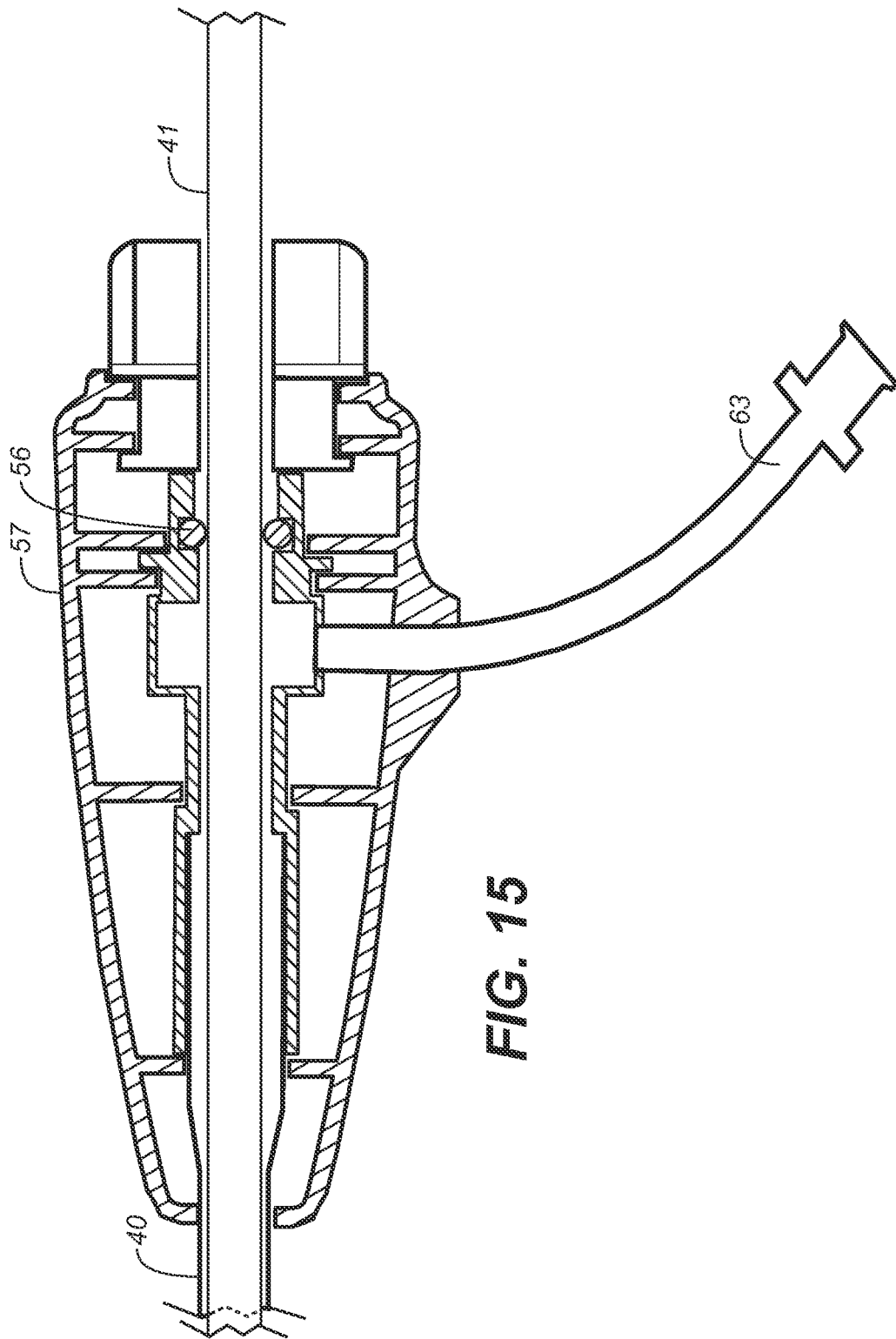
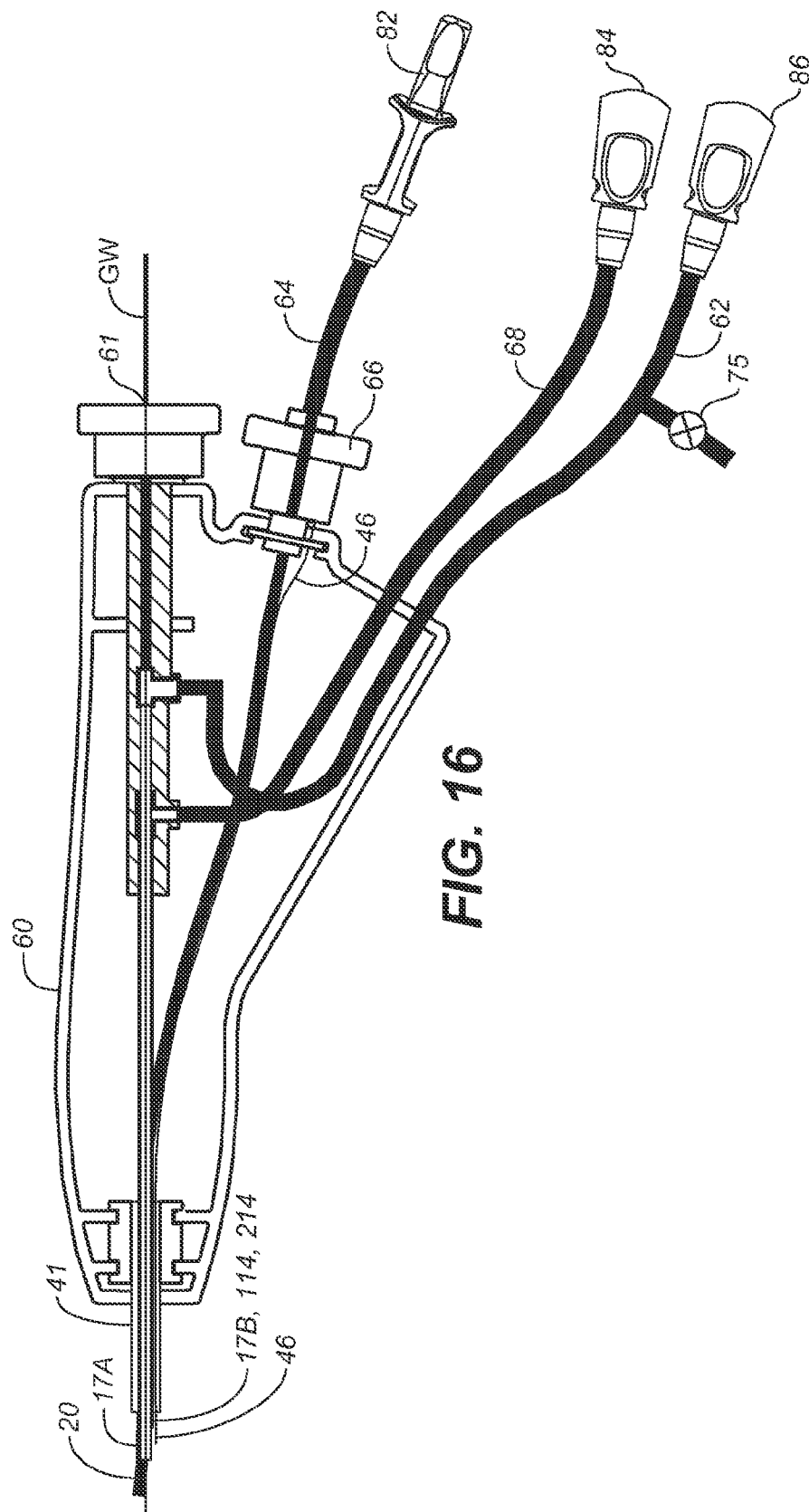
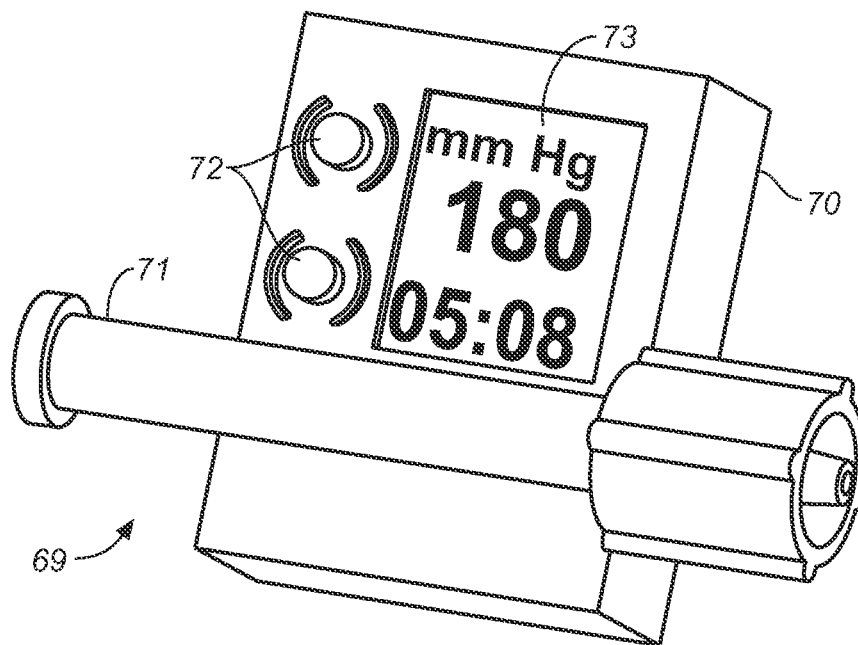


FIG. 14





**FIG. 17**

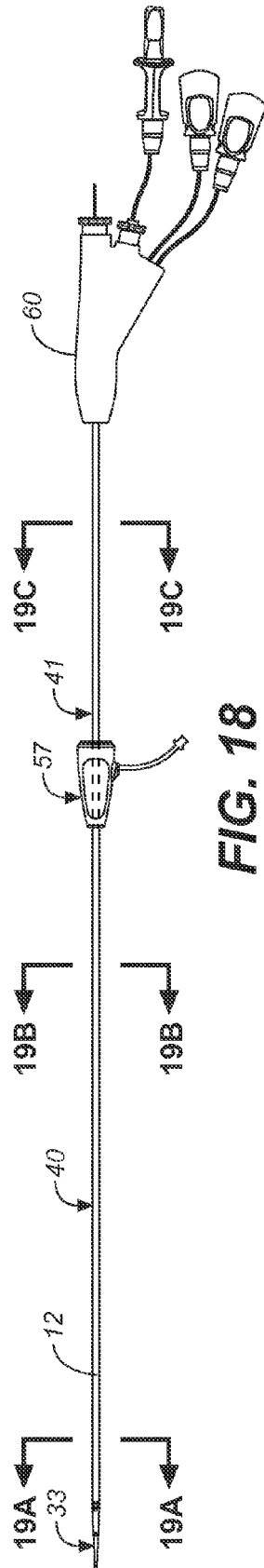


FIG. 18

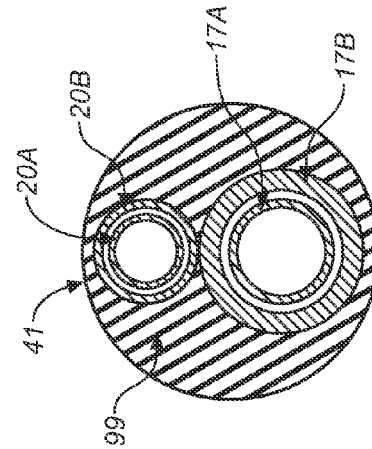


FIG. 19C

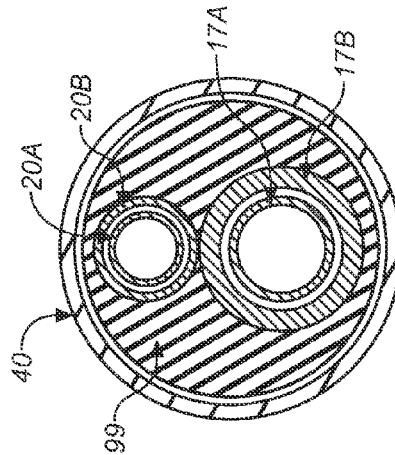


FIG. 19B

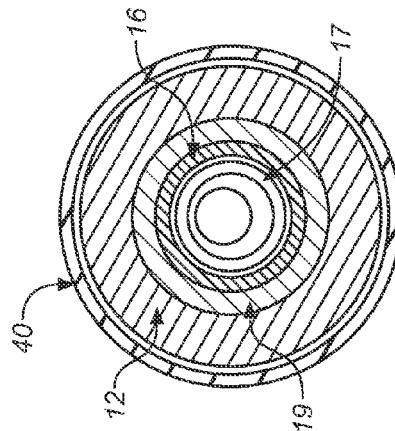


FIG. 19A

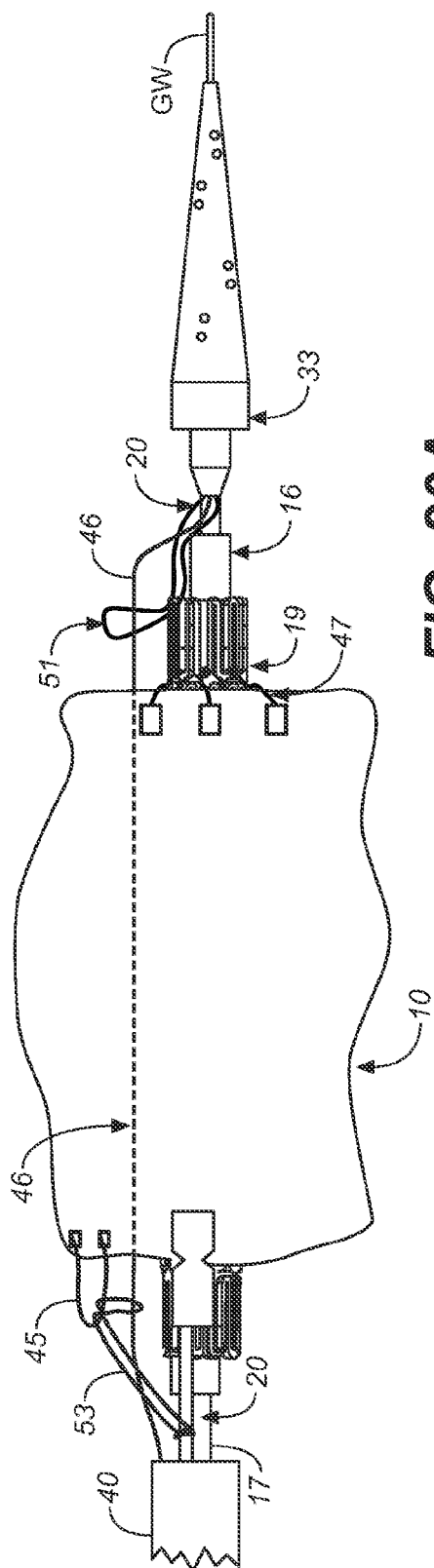


FIG. 20A

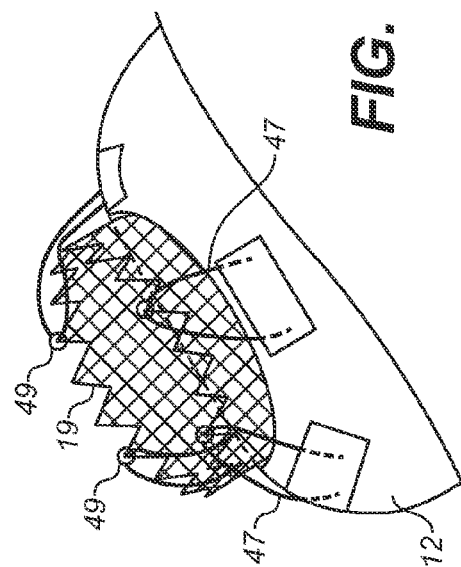


FIG. 20B

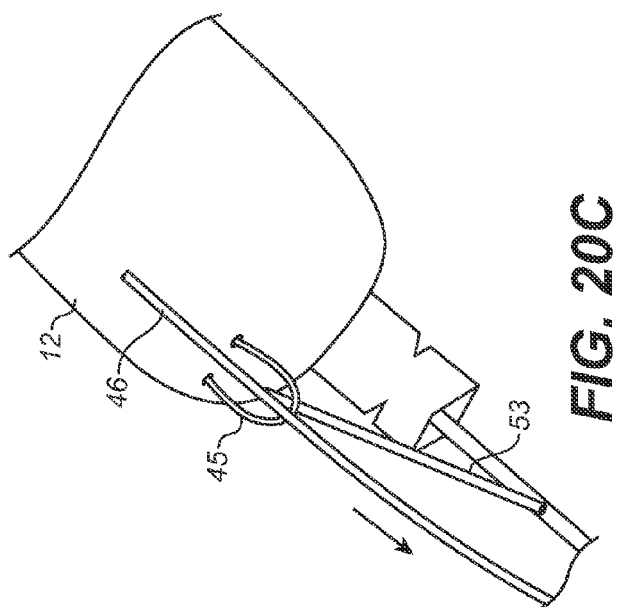


FIG. 20C

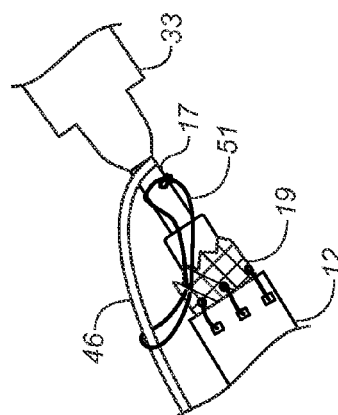


FIG. 20D

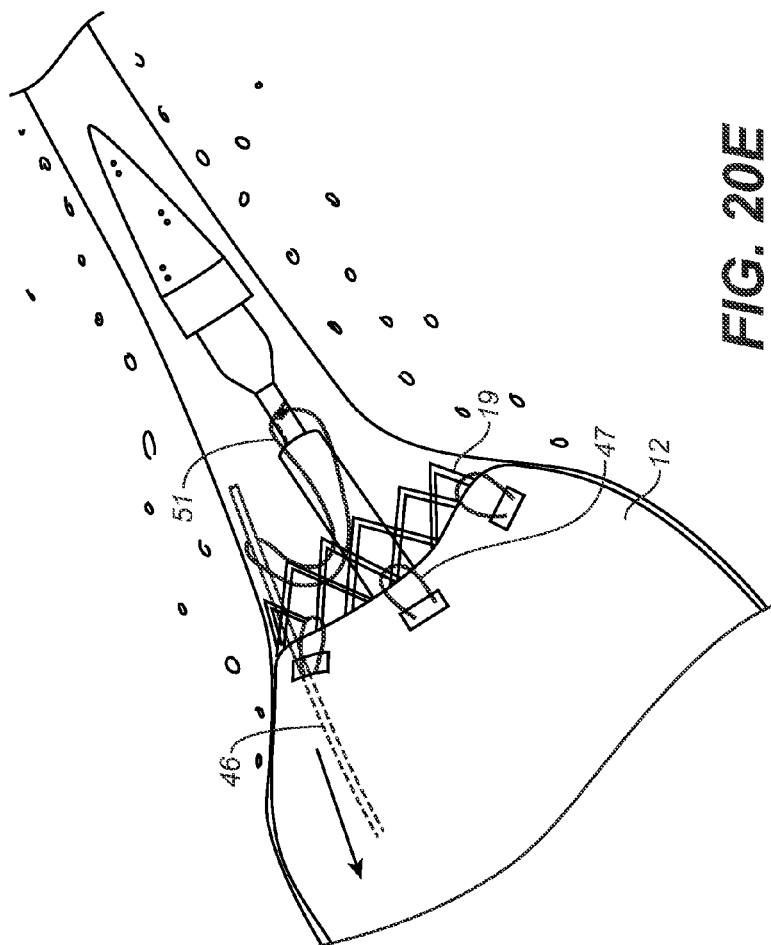
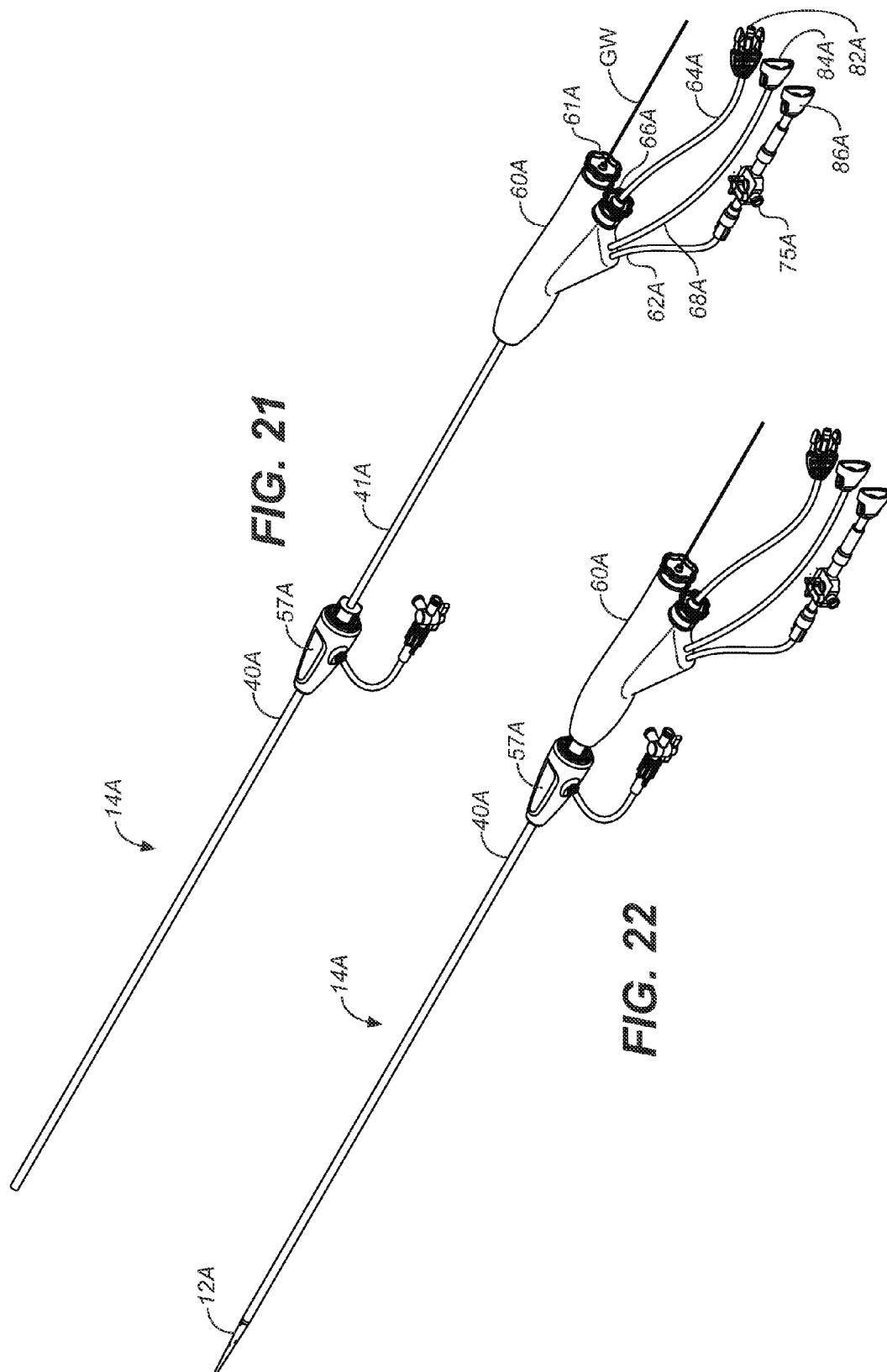
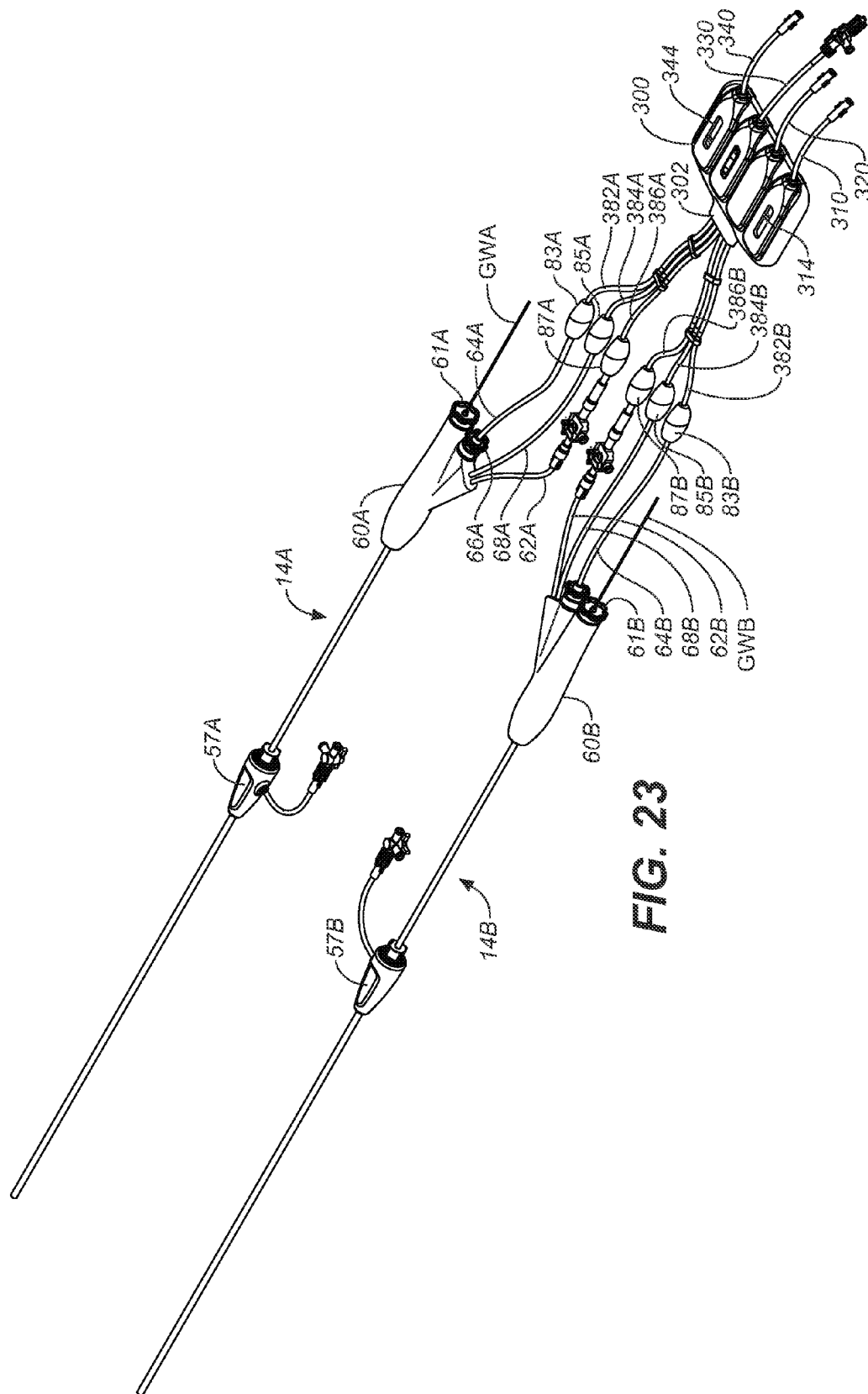
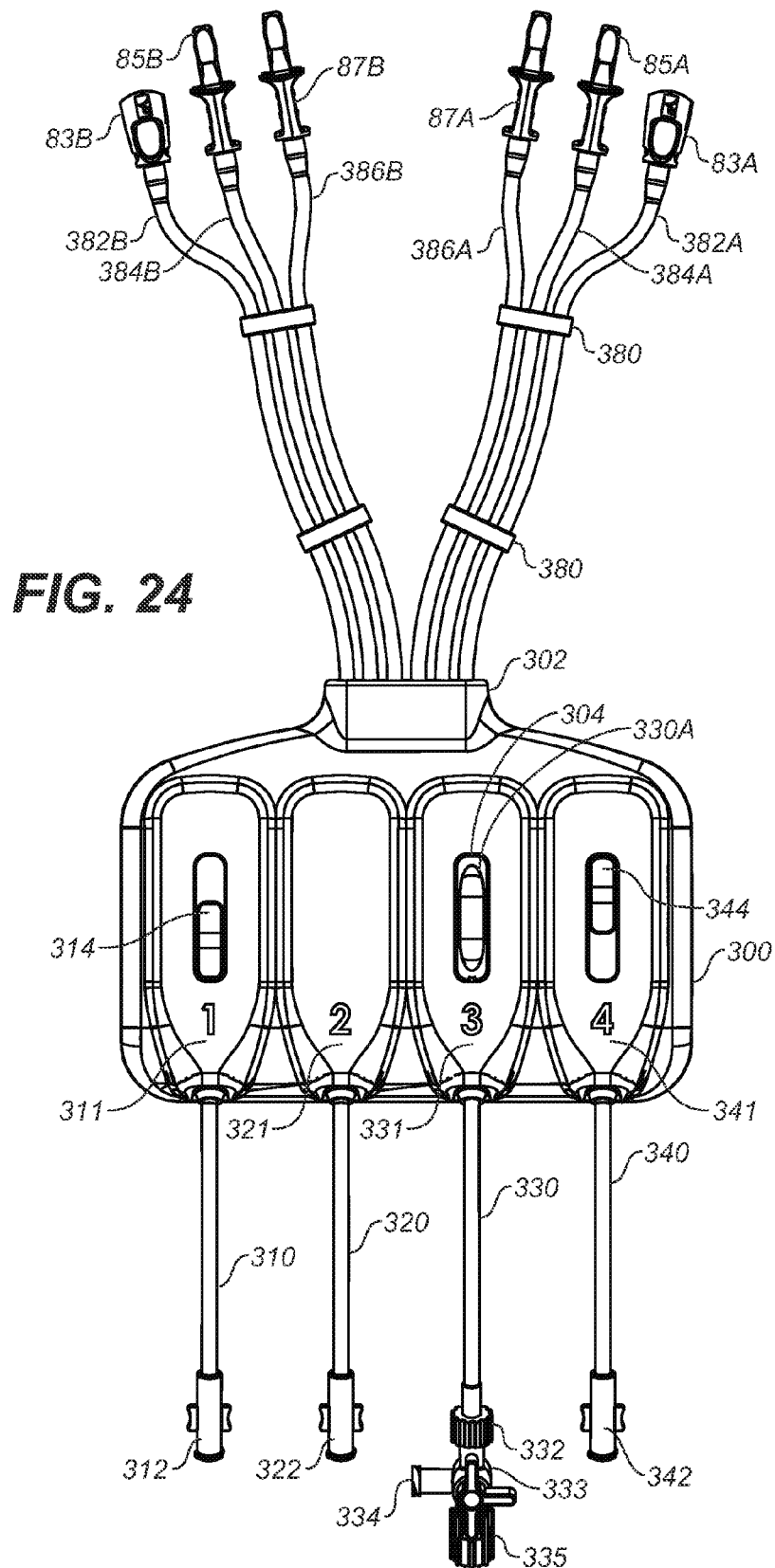
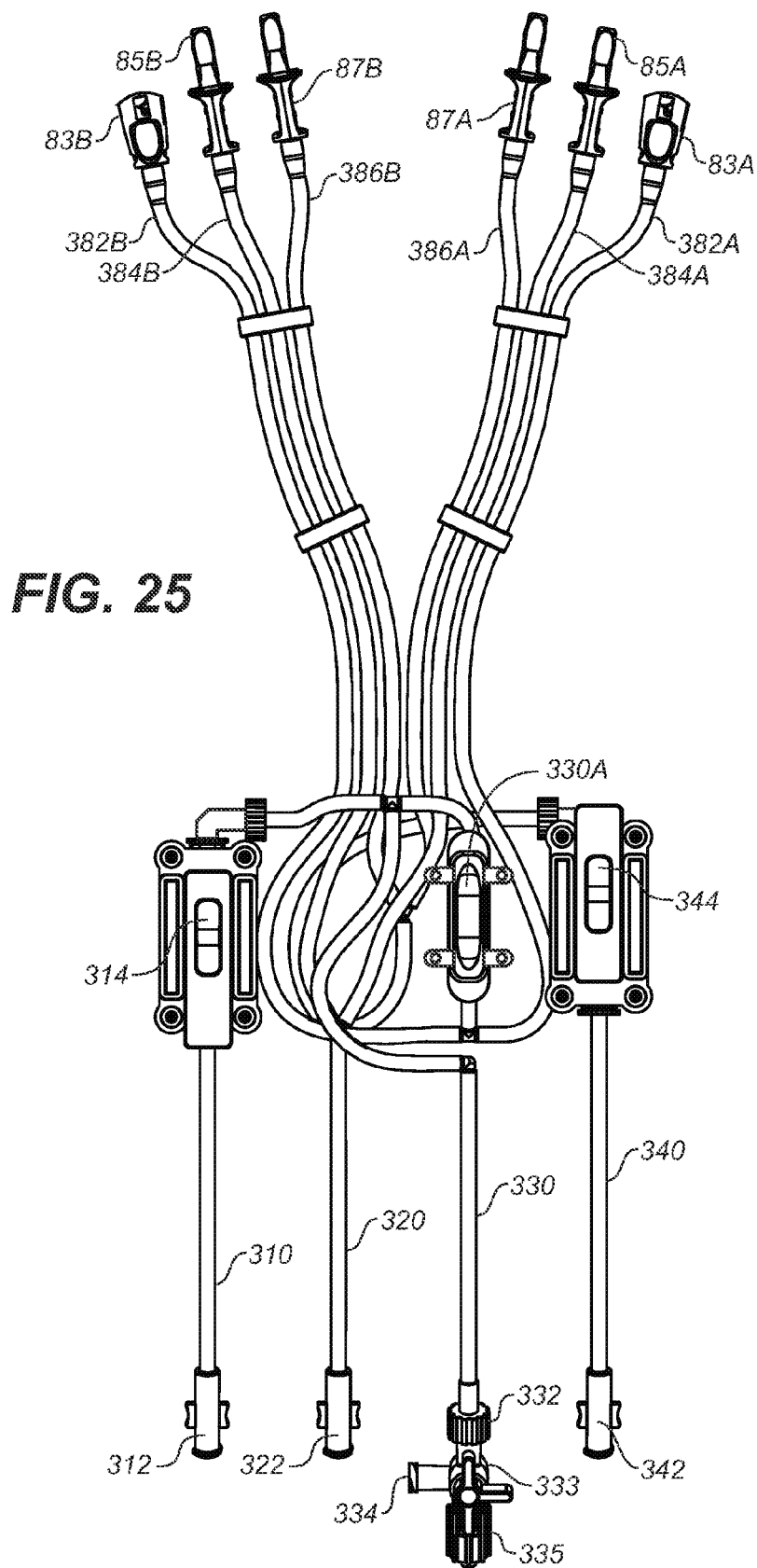


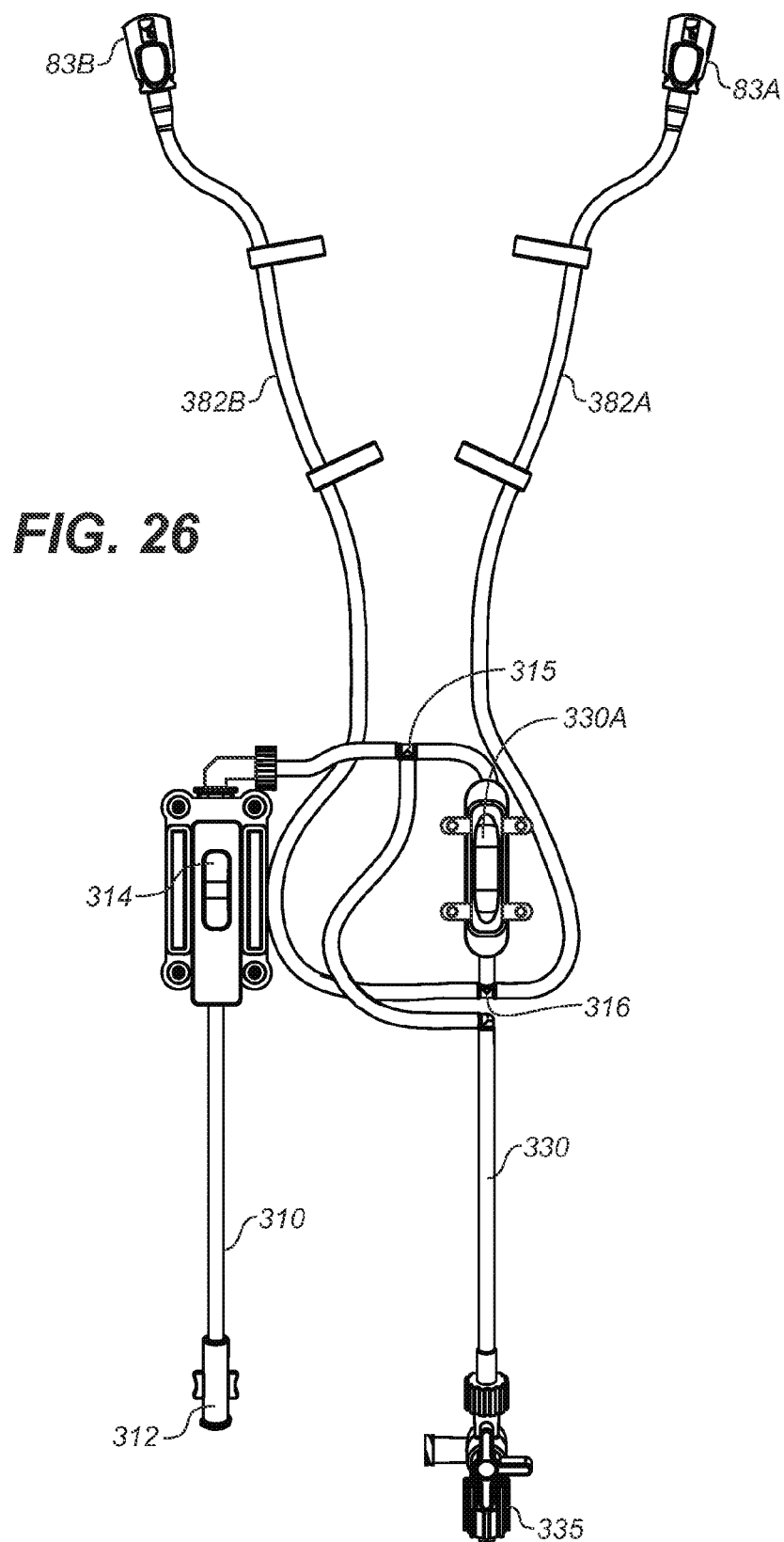
FIG. 20E

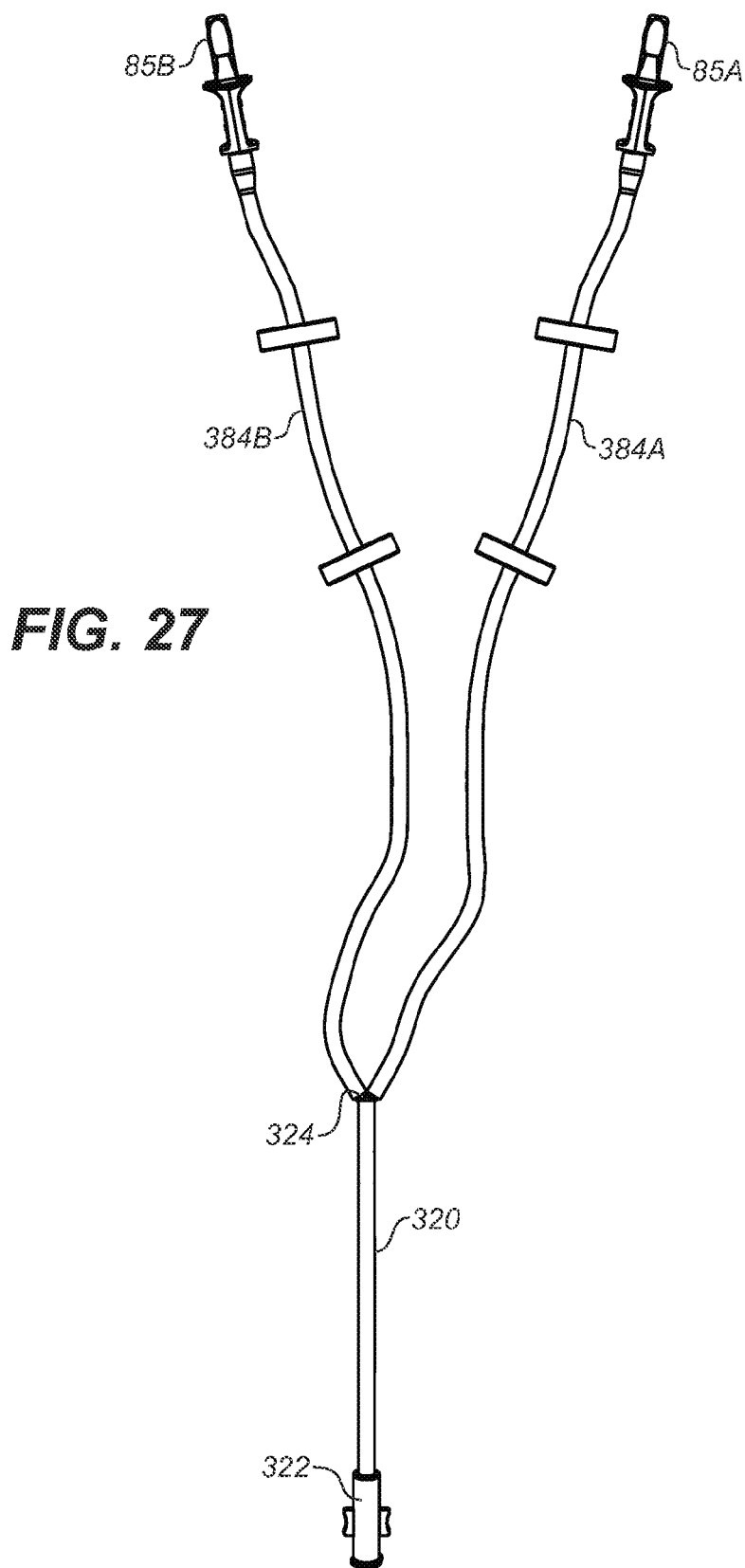












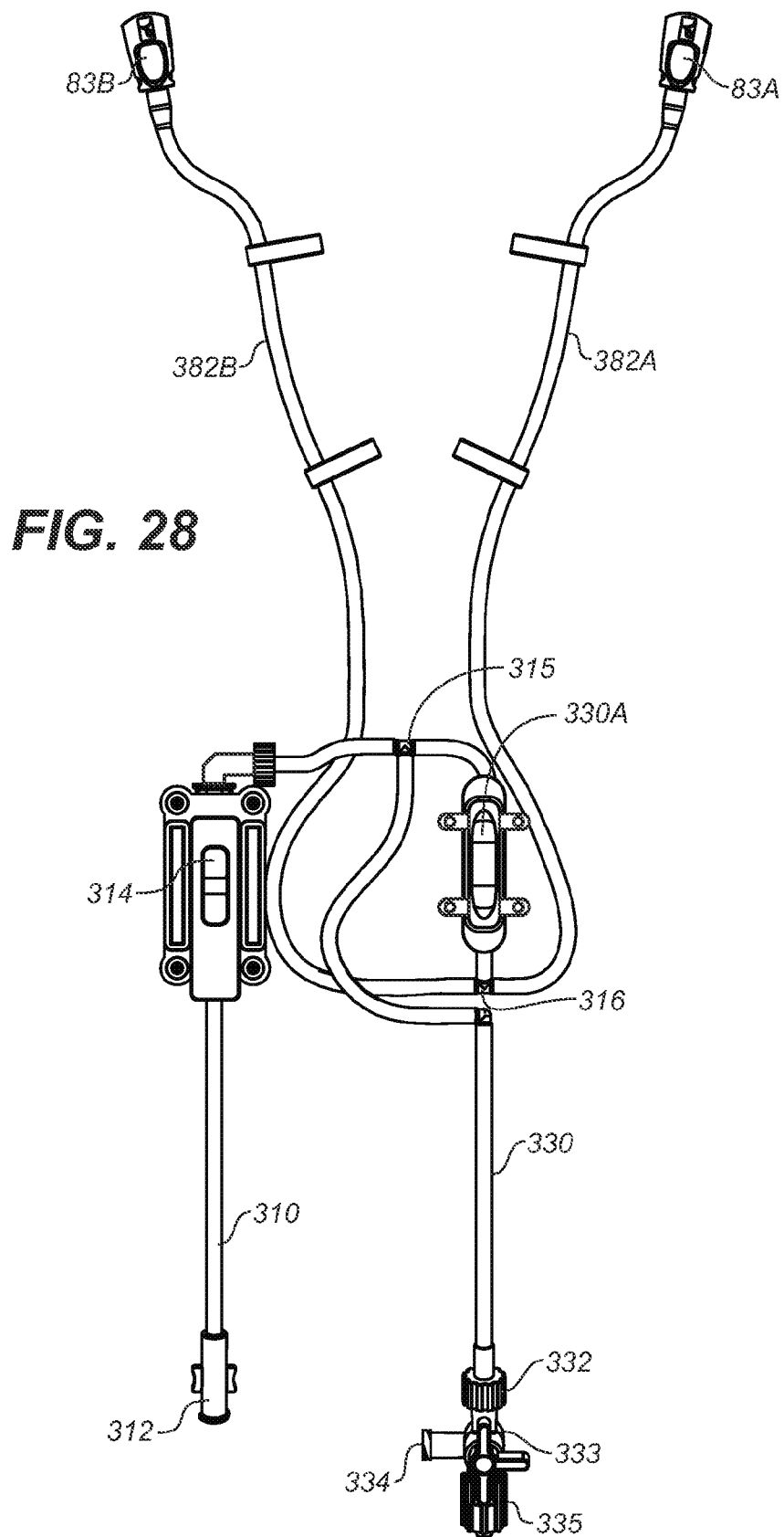
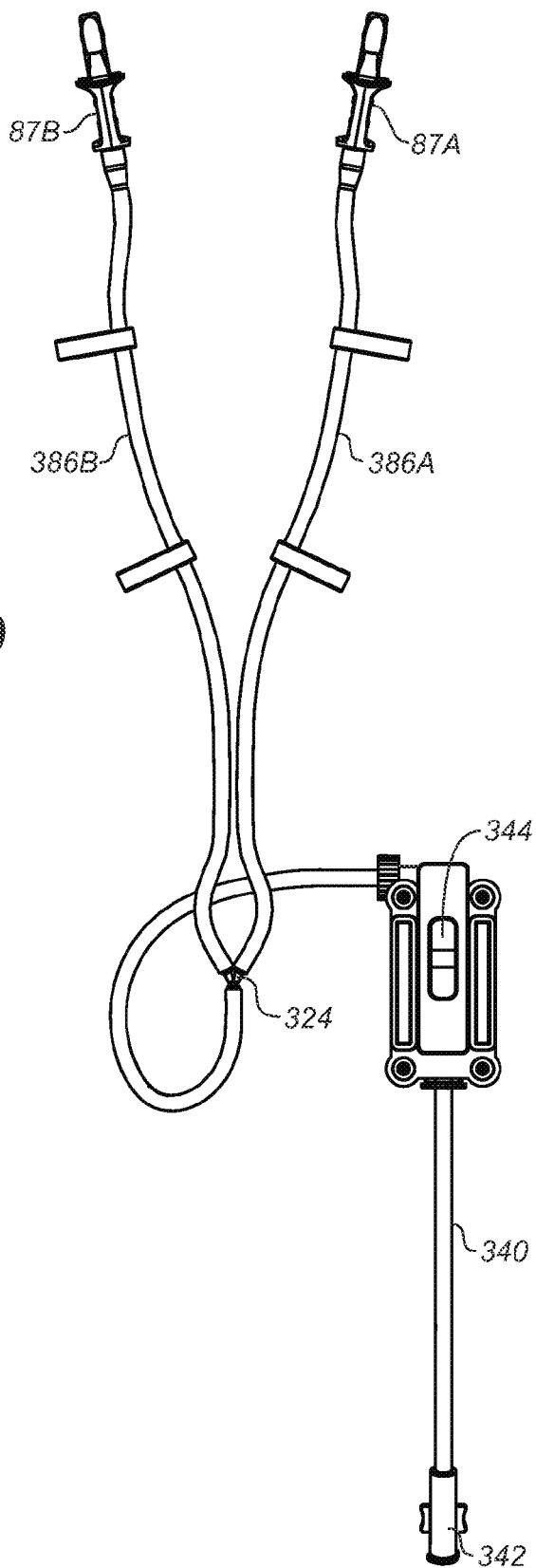


FIG. 29



1

METHOD AND SYSTEM FOR TREATING ANEURYSMS

CROSS-REFERENCES TO RELATED APPLICATIONS

This application references and claims priority from U.S. provisional patent applications 61/472,209 and 61/473,051, filed on Apr. 6, 2011 and Apr. 7, 2011, respectively, which are incorporated herein by reference in their entirety.

BACKGROUND

1. Field of the Invention

Medical apparatus and methods for treatment related to expandable prosthesis and methods for treating abdominal and other aneurysms are disclosed.

Aneurysms are enlargements or “bulges” in blood vessels which are often prone to rupture and which therefore present a serious risk to the patient. Aneurysms may occur in any blood vessel but are of particular concern when they occur in the cerebral vasculature or the patient’s aorta.

There is concern about aneurysms occurring in the aorta, particularly those referred to as aortic aneurysms. Abdominal aortic aneurysms (AAA’s) are classified based on their location within the aorta as well as their shape and complexity. Aneurysms which are found below the renal arteries are referred to as infrarenal abdominal aortic aneurysms. Supra-renal abdominal aortic aneurysms occur above the renal arteries, while thoracic aortic aneurysms (TAA’s) occur in the ascending, transverse, or descending part of the upper aorta.

Infrarenal aneurysms are the most common, representing about seventy percent (70%) of all aortic aneurysms. Supra-renal aneurysms are less common, representing about 20% of the aortic aneurysms. Thoracic aortic aneurysms are the least common and often the most difficult to treat. Most endovascular systems are also too large (above 12 F) for percutaneous introduction.

The most common form of aneurysm is “fusiform,” where the enlargement extends about the entire aortic circumference. Less commonly, the aneurysms may be characterized by a bulge on one side of the blood vessel attached at a narrow neck. Thoracic aortic aneurysms are often dissecting aneurysms caused by hemorrhagic separation in the aortic wall, usually within the medial layer. The most common treatment for each of these types and forms of aneurysm is open surgical repair. Open surgical repair is quite successful in patients who are otherwise reasonably healthy and free from significant co-morbidities. Such open surgical procedures are problematic, however, since access to the abdominal and thoracic aortas is difficult to obtain and because the aorta must be clamped off, placing significant strain on the patient’s heart.

Over the past decade, endoluminal grafts have come into widespread use for the treatment of aortic aneurysm in patients who cannot undergo open surgical procedures. In general, endoluminal repairs access the aneurysm “endoluminally” through either or both iliac arteries in the groin. The grafts, which typically have been fabric or membrane tubes supported and attached by various stent structures, are then implanted, typically requiring several pieces or modules to be assembled in situ. Successful endoluminal procedures have a much shorter recovery period than open surgical procedures.

Present endoluminal aortic aneurysm repairs, however, suffer from a number of limitations. A significant number of endoluminal repair patients experience leakage at the proximal juncture (attachment point closest to the heart) within two years of the initial repair procedure. While such leaks can

2

often be fixed by further endoluminal procedures, the need to have such follow-up treatments significantly increases cost and is certainly undesirable for the patient. A less common but more serious problem has been graft migration. In instances where the graft migrates or slips from its intended position, open surgical repair is required. This is a particular problem since the patients receiving the endoluminal grafts are those who are not considered good candidates for open surgery. Further shortcomings of the present endoluminal graft systems relate to both deployment and configuration. Multiple component treatment systems require additional procedure time to allow for introduction of each piece and even more time for assembling the pieces in situ. Such techniques are not only more time consuming, they are also more technically challenging, increasing the risk of failure. Current devices are also unsuitable for treating many geometrically complex aneurysms, particularly infrarenal aneurysms with little space between the renal arteries and the upper end of the aneurysm, referred to as short-neck or no-neck aneurysms. Aneurysms having tortuous geometries, are also difficult to treat.

For these reasons, it would be desirable to provide improved methods, systems, and prosthesis for the endoluminal treatment of aortic aneurysms. Such improved methods, systems, and treatments should provide implanted prosthesis which result in minimal or no endoleaks, which resist migration, which are relatively easy to deploy, which have a low introduction profile (preferably below 12 F), and which can treat most or all aneurysmal configurations, including short-neck and no-neck aneurysms as well as those with highly irregular and asymmetric geometries.

2. Description of the Background Art

Grafts and endografts having fillable components are described in U.S. Pat. Nos. 4,641,653; 5,530,528; 5,665,117; 5,769,882; and 7,530,988; U.S. Patent Publication 2004/0116997; and PCT Publications WO 00/51522 and WO 01/66038.

BRIEF SUMMARY OF THE INVENTION

Methods, systems, and apparatuses for the endoluminal treatment of aneurysms, particularly abdominal aortic aneurysms (AAA’s) and thoracic aortic aneurysms (TAA’s) are provided herein. Generally, the prostheses comprise double-walled filling structures which have outside walls that are compliant or otherwise adapted to substantially fill the enlarged bulk volume of an aneurysm, particularly a fusiform aneurysm, leaving a lumen in place for blood flow.

The double-walled filling structures will thus usually have a generally toroidal structure with an outer wall, an inner wall, a potential space or volume between the outer and inner walls to be filled with a filling medium, and a generally tubular lumen inside of the inner wall which provides the blood flow lumen after the prosthesis has been deployed. The shape of the filling structure is adapted to conform to the aneurysm being treated during deployment. The filling structure size can be chosen from among a few sizes to match the needs and dimensions that might be needed by nearly all patients for treating their particular aneurysmal as determined by using imaging and computer-aided diagnostic techniques. A family or collection of available filling structures may include different geometries and sizes (lengths and lumen diameters) so that a treating physician may select a specific filling structure to treat a particular patient based on the size and geometry of that patient’s aneurysm. By using the method and apparatuses described herein, each device can treat a large range of different sized anatomies, such that only a few different size

devices need be kept in inventory to be prepared to treat the full range of approved aortic aneurysmal disease indications. Generally, the outer wall of the filling structure conforms or is conformable to the inner surface of the aneurysm being treated, while the inner wall of the structure is substantially aligned with lumens of the blood vessels upstream and downstream of the prosthesis after the prosthesis has been deployed.

The filling structures of the prosthesis will usually be formed from a compliant material, such as silicone, polyurethane, latex, or combinations thereof.

The walls of the filling structures may consist of a single layer or may comprise multiple layers which are laminated or otherwise formed together. Different layers may comprise different materials, including both compliant and/or non-compliant materials. The walls may also be structurally reinforced in various ways, including use of braided reinforcement layers, filament reinforcement layers, and the like. In some embodiments, the system may include self-expanding scaffolds within the filling structures so that the structures can be initially delivered and allowed to self-expand at the treatment site, thus obviating the need for the structures associated with a balloon delivery catheter as described below.

In many embodiments, delivery protocols described utilize delivery catheters having a balloon or other expandable support for carrying the filling structure. When using balloons, the balloons may be substantially or entirely compliant, although non-compliant and combination compliant/non-compliant balloons may also be used. The balloon or other mechanical expansion components of the delivery catheter will initially be disposed within the inner tubular lumen of the filling structure, with the filling structure generally being collapsed into a low width or low profile configuration over the expansion element. The delivery catheter may then be introduced intraluminally, typically into each iliac artery and upwardly to the region within the aorta to be treated. Such delivery catheters may also include one or more lumens, tubes, or other components or structures for delivering the filling medium in a fluid form to an internal filling cavity of the filling structure. Thus, the delivery catheters can be used to both initially place and locate the filling structure of the prosthesis at the aneurysmal site. Once at the aneurysmal site, the internal tubular lumens of the structures can be expanded simultaneously using the balloons or other expandable elements on the delivery catheters. The filling structures (separate from the expansion of the tubular lumen) will be filled and expanded by delivering the filling medium via the catheters into the internal volume of the filling structures. Generally, both expansion and filling operations are performed simultaneously for a reliable and consistently predictable treatment result, or can be individually expanded in either order, e.g. the filling structure may be filled first with the delivery catheter balloon being expanded second, or vice versa, as desired or if simultaneous expansion and filling can for some reason not be performed. The filling structure(s) and/or delivery balloons may have radiopaque markers to facilitate placement and/or pressure sensors for monitoring filling and inflation pressures during deployment. The simultaneous filling allows structures to automatically accommodate one another and does not require the operator take extra special care as is often necessary when pressurization of adjacent separate structures is done separately and not simultaneously from a common source.

As described below, the filling structure may be filled with filling medium at a pressure from 100 mm of Hg to 330 mm of Hg, as needed to achieve or slightly exceed the patient's systolic blood pressure to have the fill bag displace the blood

already in the circulatory system; too high a pressure in a compliant balloon can create excess stress on the already weakened aneurysmal wall, thus should be avoided. The above pressures are gage pressures, i.e. measured relative to atmospheric pressure.

The sequential delivery of two prostheses and their respective filling structures may be utilized to initiate treatment of aneurysms located adjacent a vessel bifurcation, such as infrarenal abdominal aortic aneurysms. Two filling structures are introduced in a generally adjacent, parallel arrangement within and substantially spanning the aneurysmal volume and sac. In the specific case of infrarenal aneurysms, each prosthesis is typically delivered separately, one through each of the two iliac arteries. After locating the filling structures of the prosthesis within the aneurysmal space, to achieve an optimal result, they can be filled simultaneously using a pressurization manifold console, particularly a single operator pressurization manifold console, so as to fill and occupy substantially the entire aneurysmal volume, forming a pair of blood flow lumens spanning the aneurysmal sac.

Suitable filling materials typically include a fluid (often having a low viscosity), at least initially, to permit delivery through connected piping in the delivery catheter and may be curable or otherwise hardenable so that, once in place, the filling structure forms a final shape which will remain after the delivery catheter is removed. The fillable materials will usually be curable polymers which, after curing, will have a fixed shape with a Shore hardness typically in the range from 10 durometer to 140 durometer. The polymers may be delivered as liquids, gels, foams, slurries, or the like. The polymers may be epoxies or other curable two-part systems. In other embodiments, the polymer may comprise a single material which when exposed to the vascular environment within the filling structure changes state over time, typically from zero to ten minutes.

After curing, the filling material may have a specific gravity, typically in the range from 0.1 to 5, more typically from 0.8 to 1.2 which is generally the same as blood or thrombus. The filling material may also include bulking and other agents to modify density, viscosity, mechanical characteristics or the like, including microspheres, fibers, powders, gasses, radio-paque materials, drugs, and the like. Exemplary filling materials include polyurethanes, collagen, polyethylene glycols, microspheres, and the like.

Preferably, the filling structures of the prosthesis will require no additional sealing or anchoring means to hold them in place within the aneurysm. In some instances, however, it may be desirable to employ additional sealing or anchoring mechanisms, such as stents, scaffolds, hooks, barbs, sealing cuffs, and the like. For sealing cuffs or stents which extend proximally of infrarenal prosthesis, it may be desirable to provide openings or ports to allow the anchoring or sealing devices to extend over the renal ostia while penetrating blood flow into the renal arteries. The sealing or anchoring devices typically attach to and/or overlap with the filling structure of the prosthesis and provide for a smooth transition from the aortic and/or iliac lumens into the tubular lumens provided by the deployed filling structures.

The filling structures may be modified in a variety of ways. For example, the external surfaces of the filling structures may be partially or entirely modified to enhance placement within the aneurysmal space, typically by promoting tissue ingrowth or mechanically interlocking with the inner surface of the aneurysm. Such surface modifications include surface roughening, surface stippling, surface flocking, fibers disposed over the surface, foam layers disposed over the surface, rings, and the like. The filling structures may also include

5

biologically active substances over all or a portion of the external surface of the filling structure, such as thrombogenic substances, tissue growth promotants, biological adhesives, and the like. The filling structures may further include synthetic adhesives, such as polyacrylamides, over the surface to enhance adherence.

In some applications, it may be desirable to modify all or a portion of the internal surface of the filling cavity of the filling structure. Such surface modifications may comprise surface roughening, rings, stipples, flocking, foam layers, fibers, adhesives, and the like. The purpose of such surface modification is usually be to enhance the filling and bonding to the filling material, and to control the minimum wall thickness when the structure is filled particularly after the filling material has been cured. In particular instances, such as in locations of the filling structure which are pressed together when the structure is deployed, thus potentially excluding filling material, it may be desirable if the surfaces of the filling structure adhere directly to each other.

In view of the above general description, specific embodiments are described and discussed herein. Methods for treating an aneurysm comprise positioning at least two double-walled filling structures across the aneurysm. By "across" the aneurysm, it is meant generally that the filling structure will extend axially from one anatomical location which has been identified by imaging or otherwise as being the beginning of the aneurysm to a second location (or locations in the case of bifurcated aneurysm) where it has been similarly established that the aneurysm ends. After positioning, the two filling structures are filled simultaneously by using a manifold console, particularly a single operator manifold console, to which the filling lines for the structures are securely coupled so that a fluid filling medium is supplied and causes an outer wall of the structure to expand and conform to the inside of the aneurysm and its complementary companion structure and an inner wall of the structures form generally tubular lumens to provide for blood flow after the filling structures have been deployed. The tubular lumens will preferably be supported, typically by a balloon or mechanically expandable element, while the filling structures are being filled, after the filling structures have been filled, or during both periods. After the filling structures have been filled, the filling material or medium is hardened while the tubular lumens remain supported. Supporting the tubular lumens during hardening assures that the lumens have a desired geometry, properly align with adjacent vascular lumens, and that the tubular lumens being formed remains aligned with the native aortic and/or iliac artery lumens after the prostheses have been fully implanted. The support may be provided by a balloon which extends proximally and distally of the filling structure where the balloon may slightly "overexpand" in order to assure the desired smooth transition and conformance of the tubular lumen provided by the filling structure with the native vessel lumens.

After hardening, the support (such as an endoframe) may be left in place, (if not obstructing blood flow) or may be removed, leaving the filling structure in place. In most instances, however, prior to hardening, it will be desirable to confirm proper placement of the filling structure. This can be done using imaging techniques or otherwise testing for patency and continuity. In some instances, it may be desirable to first fill the filling structure with saline or other non-hardenable substance to make sure that the geometry of the filling structure is appropriate for the patient being treated. After testing, the saline may be removed and replaced with the hardenable filler. Through the use of only a few sizes to cover most aneurysmal configurations, the use of a step of prefilling

6

the filling structure with saline and the time expenditure associated with such a step can be avoided.

Treating abdominal aortic aneurysms may comprise use of a first double-walled filling structure and a second double-walled filling structure. The first and second filling structures are adapted to be simultaneously filled with a hardenable filling medium while they positioned adjacent to each other within the aneurysm. The systems further comprise first and second delivery catheters which can be used to align each of the first and second filling structures properly with the right and left iliacs and the infrarenal aorta as they are being deployed, filled, and hardened.

Thus a method for treating an aneurysm includes the steps of: positioning at least two double-walled filling structures having an aneurysm conforming outer wall and a blood transit lumen creating inner wall through two separate arteries across the one aneurysm to be treated; supporting the inner walls of the blood transit lumens with a support structure; causing the support structure to expand wherein each expanded support structure defines the shape of a corresponding expanded blood transit lumen; simultaneously filling the filling structures with a fluid filling medium so that their outer walls conform to the inside of the aneurysm and to each other thereby creating a blood transit barrier substantially filling the bulk volume of the aneurysm and substantially preventing blood transit between the aneurysm conforming outer wall and the inside of the aneurysm and the inner walls surround the expanded support structure to contain blood in each corresponding expanded blood transit lumen; hardening the filling medium; and removing fill lines connected to each of the double-walled filling structures after the fluid filling medium has hardened, wherein the fluid filling structure is filled with fluid filling medium at a filling pressure exceeding the systolic blood pressure experienced by the aneurysm and wherein the expanded support structure provides an outward force which is greater than the inward force applied by the filling pressure. The support structure may be an endoframe. The filling pressure may be in the range from 100 mm Hg to 330 mm Hg. The fluid filling medium can be a flowable polymer which is curable in situ. The polymer can be a polyurethane, a polyethylene glycol, or a collagen. The fluid filling medium can have a density in the range from 0.1 gm/cc to 5 gm/cc when hardened. The fluid filling medium comprises a two-part curable material which hardens after mixing. The method may include positioning an anchor or sealing element within at least one opening of the tubular lumen of the filling structure, wherein the anchor or sealing element extends from the lumen of the filling structure into a lumen of the blood vessel and/or positioning an anchor or sealing element at each opening.

Another method for treating an abdominal aortic aneurysm between the iliacs and the renal arteries, includes: positioning a first double-walled filling structure on a first endoframe from one iliac artery and artery access site, across the aneurysm, and into the aorta beneath the renal arteries, wherein the first endoframe shapes the entire length of a first tubular lumen; positioning a second double-walled filling structure on a second endoframe from the other iliac artery and artery access site, across the aneurysm, and into the aorta beneath the renal arteries and adjacent to the first double-walled filling structure, wherein the second endoframe shapes the entire length of a second tubular lumen; causing the first endoframe and the second endoframe to be expanded to create a first expanded tubular lumen and a second expanded tubular lumen; simultaneously filling the first filling structure and the second filling structure with a fluid filling medium so that an outer wall of the first filling structure and the second filling

structure conform to an inside surface of the aneurysm and the first filling structure and second filling structure conform to each other and an inner wall of the first filling structure and the second filling structure each form a generally tubular lumen with a shape defined by the expanded first tubular lumen and the expanded second tubular lumen from the first iliac and the second iliac to the aorta beneath the renal arteries; simultaneously hardening the fluid filling medium in the first filling structure and the second filling structure while the first endo-
 5 frame continues to define the shape of the expanded first tubular lumen and the second endo-
 10 frame continues to define the shape of the expanded second tubular lumen. The first and the second endoframes may extend upstream and downstream from each double-walled filling structure of the first filling structure and the second filling structure so that each
 15 endo-
 frame aligns and conforms each end of the filling structure with the iliac and aorta. An outer wall of the first filling structure or the second filling structure may be formed from a compliant material and/or from a non-compliant material or a combination thereof. Each endo-
 20 frame can include a mechanical structure expandable to one or more fixed diameters. Each filling structure can be filled with fluid filling medium at filling pressure and each expanded endo-
 frame resists the force of the filling pressure surrounding it and maintains the expanded shapes of the first and second tubular lumens. The
 25 filling pressure may be in the range from 100 mm Hg to 330 mm Hg. An anchor or sealing element may be positioned at one or more openings from the tubular lumen of at least one of the filling structures to a lumen of the iliac or aorta.

Another method of treating an aortic aneurysm using two
 30 catheters each having a sheath holding compressed within one or more expandable endobags in fluid communication with one another and an endobag fill line surrounding a compressed endo-
 frame includes the steps of: threading a catheter into each of two separate femoral arteries of a patient to be
 35 treated and into the aorta with a common end of each endo-
 frame of the catheters being positioned near a proximal end of an aneurysmal sac of the aneurysm to be treated, wherein the proximal ends of the endoframes of each of the catheters are
 40 positioned adjacent one another in anticipation of expansion of the endoframes of each of the adjacent catheters in a configuration ensuring substantially unobstructed blood flow through each lumen of the expanded endoframes; wherein the common end of the endoframes are at the substantially the
 45 same level and at a location in the aorta adjacent to where landing of the common ends of the endoframes is intended; removing the sheath exposing the expandable endobag and expanding the compressed endo-
 frame of each of the two catheters; establishing communication between a fill line for an expandable endobag of a first of the two catheters and a fill
 50 line for an expandable endobag of a second of the two catheters and a curable filler material source to form an endobag filler circuit; monitoring and controlling the pressure within the endobag filler circuit while using one source of curable
 55 filler material to pressurize the endobag filler circuit thereby simultaneously pressurizing the fill line for each expandable endobag of the two catheters causing the expandable endobags disposed across the aneurysm within the patient to inflate to fill the aneurysm and press against each other and the aneurysmal wall, wherein controlling the pressure within
 60 the endobag filler circuit consists of filling of the endobag filler circuit until the maximum pressure reading monitored during pressurization is at least equal to the systolic blood pressure of the patient being treated, wherein the maximum pressure reading monitored during pressurization is estab-
 65 lished when curable filler material injection causing the pressurizing of the endobag filler circuit is stopped and steady

state endobag circuit pressure is measured; maintaining the pressure within the endobag filler circuit for a curing time allowing the curable filler material to cure; detaching the endobag fill lines from their respective endobags and removing the two catheters from the patient.

A system for treating an aneurysm includes: a first catheter and a second catheter each catheter having a double-walled filling structure with an aneurysm conforming outer wall and a blood transit lumen creating inner wall, known as an endobag, surrounding an endo-
 10 frame releasably coupled to the catheter and held compressed in an unexpanded configuration by a retractable sheath, wherein an endobag pressurization piping has one end releasably coupled to the endobag and has an inner lumen in communication with the inside of the
 15 endobag with the other end of the endobag pressurization piping extending within the sheath and in communication with endobag pressurization tubing outside the catheter, wherein an inside of an endo-
 frame expanding substantially non-compliant balloon is in communication with endo-
 20 frame pressurization tubing outside of the catheter, and wherein a guidewire lumen of the catheter is in communication with guidewire lumen pressurization tubing extending outside of the catheter; a single operator sequential manifold console having two endobag pressurization tubing outlet ports, two
 25 endo-
 frame pressurization tubing outlet ports, and two guidewire lumen pressurization outlet ports wherein one of the two ports are connectable to the ends of the corresponding pressurization tubing outside of both the first catheter and the second catheter; the manifold console further having sequen-
 30 tial inlet ports, wherein a first inlet port communicates with the two endobag pressurization tubing outlet ports, wherein a second inlet port communicates with the two endo-
 frame pressurization tubing outlet ports, and wherein a third inlet port communicates with the two guidewire lumen pressurization
 35 outlet ports, wherein when the tubing ends from the first and the second catheters are connected to the corresponding manifold console outlet ports, pressurization of the corresponding inlet port equally pressurizes the corresponding pressure containing passage in both the first catheter and the second catheter simultaneously; wherein the first, second, and third inlet ports are configured in a side by side sequential configuration, where the sequential configuration of first, sec-
 40 ond, and third ports is arranged to match a recommended sequence of an operator's steps of pressure application to the first and second catheter endobag pressurization, endo-
 45 frame pressurization, and guidewire lumen pressurization tubing. The single operator sequential manifold console may include a polymer cured indicator comprising a colored surface facing a light transmissive section of the endobag pressurization
 50 piping along the polymer flow path of the piping between the endobag pressurization inlet port and the two endobag pressurization outlet ports, such that the color of the colored surface can be seen through the light transmissive section of the piping when the piping is empty or is pressurized to contain uncured polymer and that the color of the colored surface is at least partially obstructed by a change in light transmissivity of the polymer as it cures thereby providing a visual confirmation, by the obstruction of viewing of the colored surface to the operator of the state of cure of the polymer. The single operator sequential manifold console may also include a fourth inlet port, which is also in communication with the endobag pressurization piping in the manifold console, where the fourth port is not located adjacent the first inlet port. The single operator sequential manifold console may include a fourth inlet port flow valve which when closed prevents flow between the endobag pressurization piping in the sequential manifold console and the fourth inlet

port. The single operator sequential manifold console includes a third inlet port flow valve which when closed prevents flow between the guidewire lumen pressurization piping in the sequential manifold console and the third inlet port.

A single operator sequential manifold console may include two endobag pressurization tubing outlet ports, two endoframe pressurization tubing outlet ports, and two guidewire lumen pressurization outlet ports wherein one of the two ports are connectable to ends of corresponding pressurization tubing outside of both a first catheter and a second catheter; the manifold console further having sequential inlet ports, wherein a first inlet port communicates with the two endobag pressurization tubing outlet ports, wherein a second inlet port communicates with the two endoframe pressurization tubing outlet ports, and wherein a third inlet port communicates with the two guidewire lumen pressurization outlet ports, wherein when the tubing ends from the first and the second catheters are connected to the corresponding manifold console outlet ports, pressurization of the corresponding inlet port equally pressurizes the corresponding pressure containing passage leading to both the first catheter and the second catheter simultaneously; wherein the first, second, and third inlet ports are configured in a side by side sequential configuration, where the sequential configuration of first, second, and third ports is arranged to match a recommended sequence of an operator's steps of pressure application to the connectable first and second catheter endobag pressurization, endoframe pressurization, and guidewire lumen pressurization tubing. The single operator sequential manifold console may include a polymer cured indicator comprising a colored surface facing a light transmissive section of the endobag pressurization piping along the polymer flow path of the piping between the endobag pressurization inlet port and the two endobag pressurization outlet ports, such that the color of the colored surface can be seen through the light transmissive section of the piping when the piping is empty or is pressurized to contain uncured polymer and that the color of the colored surface is at least partially obstructed by a change in light transmissivity of the polymer as it cures thereby providing a visual confirmation, by the obstruction of viewing of the colored surface to the operator of the state of cure of the polymer. The single operator sequential manifold console may also include a fourth inlet port, which is also in communication with the endobag pressurization piping in the manifold console, where the fourth port is not located adjacent the first inlet port and which when closed prevents flow between the endobag pressurization piping in the sequential manifold console and the fourth inlet port. The single operator sequential manifold may include a third inlet port flow valve which when closed prevents flow between the guidewire lumen pressurization piping in the sequential manifold console and the third inlet port.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 illustrates an example of a single prosthesis system comprising a filling structure mounted over a delivery catheter.

FIG. 2 is a cross-sectional view of the filling structure of FIG. 1 illustrating various surface modifications and a filling valve.

FIGS. 3A-3C illustrate alternative wall structures for the filling structure.

FIG. 4 illustrates the anatomy of an infrarenal abdominal aortic aneurysm.

FIGS. 5A-5D illustrate use of the prosthesis system of FIG. 1 for treating the infrarenal abdominal aortic aneurysm.

FIG. 6 illustrates an example of a system with a pair of prosthesis for delivery to an infrarenal abdominal aortic aneurysm, where each prosthesis comprises a filling structure mounted on a delivery catheter.

FIGS. 7A-7F illustrate use of the prosthesis system of FIG. 6 for treating an infrarenal abdominal aortic aneurysm.

FIG. 8 illustrates an example of a delivery catheter shaft carrying a single prosthesis system which comprises a filling structure mounted over an endoframe structure.

FIG. 9 illustrates an example of a system comprising a pair of prostheses for delivery to an infrarenal abdominal aortic aneurysm, where each prosthesis comprises a delivery catheter shaft carrying a filling structure mounted over an endoframe structure.

FIGS. 10A-10I illustrate exemplary usage of the system of FIG. 9 for treating an infrarenal abdominal aortic aneurysm.

FIGS. 11A-11B illustrates an exemplary system having a fenestrated nosecone during advancement of the system in the vasculature and during deployment of the filling structure at the treatment site, respectively.

FIG. 12 shows an exemplary aneurysm treatment system having a fenestrated nosecone, a carrier knob and a handle.

FIG. 13 illustrates the fenestrated nosecone of the system of FIG. 12.

FIG. 14 depicts angiography as performed with the nosecone of FIG. 12.

FIG. 15 illustrates the annular carrier knob of the system of FIG. 12.

FIG. 16 illustrates the handle of the system of FIG. 12.

FIG. 17 illustrates an exemplary pressure monitor.

FIGS. 18 and 19A-19C illustrate an exemplary embodiment and cross-sections of the embodiment.

FIGS. 20A-20E illustrates exemplary coupling mechanisms of an aneurysm treatment system, in accordance with several embodiments.

FIGS. 21 and 22 show two lateral views of a catheter treatment system, the catheter of FIG. 21 is shown in its as shipped configuration, i.e., prior to initiating deployment, where the sheath retraction knob, end handle, fluid connection, and endobag release wire fittings are in their pre-deployment configuration. FIG. 22 shows a configuration of the catheter with the sheath having been retracted, i.e., after deployment has been initiated.

FIG. 23 is a lateral view showing two separate and discrete catheter treatment systems/devices as in FIG. 21, where filling structure fill tubing, endoframe/expansion balloon pressurization tubing, and a guidewire lumen flush or contrast solution supply tubing from each catheter is connected to a sequential deployment step indicating single operator manifold console used to simultaneously pressurize and operate the function of both catheters from one operating input and location.

FIG. 23 is a lateral view showing two single catheter treatment systems configure for operation with a single operator manifold console.

FIG. 24 is a plan view of the single operator manifold console of FIG. 23.

FIG. 25 is a cut-away plan view of the piping/tubing layout, showing the piping layout to, through, and out of the single operator manifold console of FIG. 24.

FIG. 26 is a cut-away diagram of the piping/tubing layout of the single operator manifold console of FIG. 24, isolating the piping system used for the application of vacuum to the endobag piping system.

11

FIG. 27 is a cut-away diagram of the piping/tubing layout of the single operator manifold console of FIG. 24, isolating the piping system used for the application of pressure and vacuum to the endoframe/balloon piping/tubing system.

FIG. 28 is a cut-away diagram of the piping/tubing layout of the single operator manifold console of FIG. 24, isolating the piping system used for the supply of pressurized polymer through the endobag pressurization piping/tubing.

FIG. 29 is a cutaway diagram of the piping layout of the single operator manifold console of FIG. 24 showing the piping/tubing layout for the application of angiography contrast solution to the catheter treatment system through the guidewire lumen.

DETAILED DESCRIPTION

A system 10 is for delivering a double-walled filling structure 12 to an aneurysm includes the filling structure and a delivery catheter 14 having an expandable element, typically an inflatable balloon 16, at its distal end. The catheter 14 will comprise a guidewire lumen 18, a balloon inflation lumen (not illustrated) or other structure for expanding other expandable components, and a filling tube 20 for delivering a filling medium or material to an internal space 22 of the double-walled filling structure 12. The internal space 22 is defined between an outer wall 24 and inner wall 26 of the filling structure. Upon inflation with the filling material or medium, the outer wall will expand radially outwardly, as shown in broken line, as will the inner wall 26, also shown in broken line. Expansion of the inner wall 26 defines an internal lumen 28. The expandable balloon 16 or other structure will be expandable to support an inner surface of the lumen 28, as also in broken line in FIG. 1.

Referring now to FIG. 2, and the various internal and external surfaces may be shaped, coated, treated, or otherwise modified, to provide for a number of potentially desirable features of the present apparatus. For example, the external surface 24' of the outer wall may be shaped to have rings, stipples, or other surface features 26' which are typically formed into the material of the structure at the time of molding, vapor deposition, or other manufacturing process. The outer surface may also be coated with materials 29 which can be adhesives, drugs, active substances, fibers, flocking, foams, or a variety of other materials. In most cases, such surface features or modifications will be intended to enhance sealing or attachment of the outer wall 24 to the inner surface of the aneurysm being treated.

The inner surface 30 of the filling volume 22 may also be modified by providing features 26', coatings, surface roughening, coated with materials 29, or a variety of other modifications. The purpose of such internal features is typically to enhance adherence of the walls to the filling material or medium as the medium is cured or otherwise hardened. In some instances, materials may be coated on all or a portion of the inside surface 30 to induce or catalyze hardening of the filling material as it is being introduced.

The double-walled filling structure 12 will typically comprise at least one valve 35 to permit the introduction of the filling material or medium into the internal volume 22 using filling tube 20. As illustrated, the valve 35 may be a simple flap valve. Other more complex ball valves, and other one-way valve structures may be provided. In other instances, two-way valve structures may be provided to permit both filling and selective emptying of the internal volume 22. In other instances, the filling tube may comprise a needle or other filling structure to pass through the valve 35 to permit both filling and removal of filling medium.

12

As illustrated in FIG. 2, the wall structure of the double-walled filling structure may be a single layer, typically molded or otherwise conventionally formed. The wall structures may also be more complex, as illustrated for example, FIGS. 3A-3C. FIG. 3A shows a multi-layered wall comprising layers 42, 43 and 44. It will be appreciated that such multiple layer structure can provide for increased strength, puncture resistance, variations in compliance and/or flexibility, differences in resistance to degradation, and the like. As shown in FIG. 3B, a single wall or multiple wall structure can be reinforced by braid, coils, or other metal or non-polymeric reinforcement layers or structures 48. As shown in FIG. 3C, the external surface 24' of the wall may be covered with drugs, fibers, protrusions, holes, active agents or other substances for a variety of purposes.

Referring now to FIG. 4, the anatomy of an infrarenal abdominal aortic aneurysm comprises the thoracic aorta (TA) having renal arteries (RA) at its distal end above the iliac arteries (IA). The abdominal aortic aneurysm (AAA) typically forms between the renal arteries (RA) and the iliac arteries (IA) and may have regions of mural thrombus (T) over portions of its inner surface (S).

Referring to FIGS. 5A-5D, the system 10 of FIG. 1 may be utilized to treat the complex geometry of the transmural abdominal aortic aneurysm (AAA) of FIG. 4 by first positioning the delivery catheter 14 to place the double-walled filling structure 12 (in its unfilled configuration) generally across the aneurysm from the region of the aorta beneath the renal arteries (RA) to a region over the iliac arteries (IA), as best seen FIG. 5A. Usually, the delivery catheter 14 will be introduced over a guidewire (GW) through a puncture in the patient's groin accessing the iliac artery by the Seldinger technique.

After the double-walled filling structure 12 is properly positioned, a hardenable inflation medium is introduced into the internal space 22 filling of the inner space 22 and expands the outer wall 24 of the structure outwardly so that it conforms to the inner surface (S) of the aneurysmal space.

Before, during, or after filling of the double-walled filling structure 12 with inflation medium, as illustrated in FIG. 5B, the balloon 16 or other expansible structure will also be inflated or expanded to open the tubular lumen defined by the interior of the inner wall 26. Commonly, a non-compliant balloon 16 will be used, typically having a maximum diameter of width which is at or slightly larger than the desired tubular lumen diameter or width through the deployed double wall filling structure 12. The filling structure 12, in contrast, may be partially or completely formed from a generally compliant material, thus allowing the non-compliant balloon 16 or other expansible structure to fully open the tubular lumen and conform the ends of the lumens to the aorta and iliac walls, as illustrated in FIG. 5C. A lower or distal end 50 of the tubular lumen may be flared to a larger diameter so that it can accommodate the openings into both of the iliac arteries (IA) as illustrated. The filling structure 12 geometry can be chosen to most closely match the particular patient geometry being treated as determined during pre-treatment planning. A balloon 16 or other expansible structure which will be shaped to preferentially open the lower distal end 50 of the tubular lumen to a larger diameter than the upper or proximal end 52 can be used.

After the filling material has been introduced to the filling structure 12, typically through the filling tube 20, the fluid filling material must be cured or otherwise hardened to provide for the permanent implant having a generally fixed structure which will remain in place in the particular aneurysmal geometry. Methods for curing or hardening the filling mate-

13

rial will depend on the nature of the filling material. For example, certain polymers may be cured by the application of energy, such as heat energy or ultraviolet light. Other polymers may be cured when exposed to body temperature, oxygen, or other conditions which cause polymerization of the fluid filling material. Still others may be mixed immediately prior to use and simply cure after a fixed time, typically minutes. Often, after the filling material has been hardened, the delivery catheter **14** may be removed and the filling structure left in place as the completed prosthetic implant.

In other cases, however, it may be desirable to further position certain seals, anchors, stents, or other additional prosthetic components at either the proximal end **52** or distal end **50** of the graft. As illustrated in FIG. **5D**, for example, a stent-like structure **160** may be planted in the upper proximal end opening of the tubular lumen of the filling structure **12** in order to help anchor the structure, help prevent intrusion of blood into the region between the outer wall **24** and inner surface (S) of the aneurysm, and to generally improve the transition from the aorta into the tubular lumen. The sealing or anchoring structure may simply comprise a stent-like component, preferably having a port or other access route to allow blood flow into the covered renal arteries (if any). Alternatively, the anchor structure could be another inflatable unit, such as the anchor described in co-pending, commonly owned application US Patent Application US2004/0116997A1, the full disclosure of which is incorporated herein by reference.

In a particular, a pair of double-walled filling structures will simultaneously be used to treat infrarenal abdominal aortic aneurysms, instead of only a single filling structure as illustrated in FIGS. **5A-5C**. A system comprising such a pair of filling structures is illustrated in FIG. **6** which includes a first filling structure **112** and a second filling structure **212**. Each of the filling structures **112** and **212** are mounted on delivery catheters **114** and **214**, respectively. The components of the filling structures **112** and **212** and delivery catheters **114** and **214** are generally the same as those described previously with respect to the single filling structure system **10** of FIG. **1**. Corresponding parts of each of the fillings structures **112** and **212** will be given identical numbers with either the **100** series base number or **200** series base number. The difference between the filling structures **112** and **212**, on the one hand, and the filling structure **12** of FIG. **1** is that the pair of filling structures may generally have slightly smaller filling volume configurations as they only need to occupy an approximately complimentary half the volume of the aneurysm which are meant to be positioned adjacent to each other within the aneurysmal space and to in combination fill that space, as will be described with specific reference to FIG. **7A-7F** below.

In treating an infrarenal abdominal aortic aneurysm using the pair of filling structures **112** and **212** illustrated in FIG. **6**, a pair of guidewires (GW) will first be introduced, one from each of the iliac arteries (IA). As illustrated in FIG. **7A**. The first delivery catheter **114** will then be positioned over one of the guidewires to position the double-walled filling structure **112** across the aortic aneurysm (AAA), as illustrated in FIG. **7B**. The second delivery catheter **214** is then delivered over the other guidewire (GW) to position the second filling structure **212** adjacent to the first filling structure **112** within the aneurysm (AAA), as illustrated in FIG. **7C**.

As discussed herein below the two filling structures and associated balloons will be expanded simultaneously, a partially filled (in process) filling condition is illustrated in FIG. **7D** where the filling structure **112** and balloon **116** are shown being simultaneously inflated to simultaneously expand to fill

14

the aneurysmal volume, as illustrated in FIG. **7D**. A completed filling is illustrated in FIG. **7E**. The upper ends of the balloons **116** and **216** will conform the tubular lumens of the filling structures against the walls of the aorta as well as against each other, while the lower ends of the balloons **116** and **216** will conform the tubular lumens into the respective iliac (IA).

After filling the filling structures **112** and **212** as illustrated in FIG. **7E**, the filling materials or medium will be cured or otherwise hardened, and the delivery catheters **114** and **214** removed, respectively. The hardened filling structures will then provide a pair of tubular lumens opening from the aorta beneath the renal arteries to the right and left iliac arteries, as shown in broken line in FIG. **7**. The ability of the filling structures **112** and **212** to conform to the inner surface (S) of the aneurysm, as shown in FIG. **7F**, helps assure that the structures will remain immobilized within the aneurysm with little or no migration. Immobilization of the filling structures **112** and **212** may be further enhanced by providing any of the surface features described above in connection with the embodiments of FIG. **2**. Optionally, and not illustrated, anchoring or sealing structures could be provided in either of the upper or proximal openings of the tubular lumens into the aorta or from either of the distal or lower openings into the respective iliac arteries.

Referring now to FIG. **8**, shows a system **10** constructed for delivering a double-walled filling structure **12** (also referred to as an endograft in this disclosure) to an aneurysm. It includes the filling structure **12** disposed over a radially expandable endoframe **19**, both of which are then mounted on a inner delivery catheter shaft **17** having an expandable element, typically an inflatable balloon **16**, near its distal end and a nosecone **33** at its distal end. Nosecone **33** may be shaped to facilitate advancement of the delivery system through the vasculature and may include a series of side ports **34** for performing angiography before, during, or after deployment of the filling structure **12**. An outer sheath **40** is slidably disposed over the inner delivery catheter shaft **17**, the distal end of which interfaces with a proximal portion of nosecone **33** so as to facilitate advancement of the system through the vasculature of the patient. Expandable element **16** traverses the entire length of the endoframe **19** so that the endoframe **19** may be radially expanded upon expansion of the expandable element balloon **16** (expanded balloon **16'** shown in broken line). Endoframe **19** traverses the entire length of filling structure **12** and most of endoframe **19** is covered by filling structure **12**, however, endoframe **19** may also have proximal and a distal regions that extend uncovered beyond the filling structure **12**. One of skill in the art will appreciate that lengths of the filling structure, endoframe and expandable element may be adjusted as required and thus the relative lengths are not limited to those disclosed above. Further details about the double-walled filling structure are disclosed in U.S. Patent Publication No. 2006/0212112 and embodiments of an endoframe are disclosed in U.S. Patent Application Publication No. 2010/0004728, both of which the entire contents are incorporated herein by reference.

The catheter **14** will comprise a guidewire lumen (not shown), a balloon inflation lumen (not shown) or other structure for expanding other expandable components, and a filling tube **20** for delivering a filling medium or material to an internal space **22** of the double-walled filling structure **12**. The internal space **22** is defined between an outer wall **24** and inner wall **26** of the filling structure. Upon inflation with the filling material or medium, the outer wall **24** will expand radially outwardly (expanded outer wall **24** shown in broken line) as will the inner wall **26** (expanded inner wall **26'** shown

15

in broken line). Expansion of the inner wall 26 defines an internal generally tubular lumen 28 through which blood flows after deployment of the filling structure in the aneurysm. The expandable balloon 16 or other structure will be expandable to correspondingly expand the endoframe 19 to provide support and to shape an inner surface of the lumen 28. In this embodiment, the expandable balloon is cylindrically shaped and therefore the generally tubular lumen 28 will also be cylindrically shaped. In other embodiments, the balloon may be pre-shaped to more precisely match the curvature of the vessel. For example, when treating an aortic aneurysm, a tapered, pre-shaped or curved balloon may be used so that the lumen substantially matches the aorta. Various balloon configurations may be used in order to match vessel tortuosity. Pre-shaped, curved or tapered balloons may be used in any of the embodiments disclosed herein in order to obtain a desired lumen shaped.

In a particular, a pair of double-walled filling structures will be used to treat infrarenal abdominal aortic aneurysms, instead of only a single filling structure as illustrated in FIG. 8. A system comprising such a pair of filling structures is illustrated in FIG. 9 which includes a first filling structure 112 and a second filling structure 212. Each of the filling structures 112 and 212 are mounted on delivery catheter inner shafts 114 and 214, respectively and each system also has a radially expandable endoframe 127, 227. Inner delivery catheter shafts 114 and 214 include fenestrated nosecones 133, 233 for performing angiography before, during or after treatment, and outer sheaths 140, 240 slidably disposed over the filling structure during advancement of the system through the vasculature along the guidewires (GW). The components of the filling structures 112 and 212, the endoframes 127, 227 and inner delivery catheter shafts 114 and 214 are generally the same as those described previously with respect to the single filling structure system 10 of FIG. 8. Corresponding parts of each of the filling systems 112 and 212 will be given identical numbers with either a 100 series number or a 200 series number. Filling structures 112 and 212 will generally be positioned adjacent each other within the aneurysmal space to fill that space, as will be described with specific reference to FIGS. 10A-10I below.

FIGS. 10A-10I illustrate an exemplary use of the system in FIG. 9 for treating an infrarenal abdominal aortic aneurysm AAA with or without mural thrombus T. After the inner delivery catheter shafts 114 and 214 are advanced so that the filling structures 112 and 212 are positioned at the treatment site, the outer sheaths 140 and 240 are retracted relative the inner catheter shaft 114 and 214. The outer sheaths 140 and 240 are slidably disposed over the filling structures 112 and 212 and the corresponding endoframes 127 and 227 disposed therein. In FIG. 10A a pair of guidewires (GW) will first be introduced preferably percutaneously or by surgical cut down, from each of the iliac arteries (IA) and advanced across the aneurysm toward the renal arteries (RA). Referring now to FIG. 10B, the first delivery catheter shaft 114 having a fenestrated nosecone 133 at its distal end and an expandable balloon 116 disposed on a distal portion will then be advanced over one of the guidewires GW to position the double-walled filling structure 112 across the aortic aneurysm (AAA) along with endoframe 127. An outer sheath 140, slidably disposed over the filling structure 112 and inner shaft 114, is retracted to expose the filling structure 112 at the target treatment site. The second inner catheter shaft 214 having expandable balloon 216 and fenestrated nosecone 233 at its distal end is then delivered over the other guidewire GW to position the second filling structure 212 adjacent to the first structure 112 across the aneurysm (AAA) along with endoframe 197, as illustrated

16

in FIG. 10C. The outer sheath 240, slidably disposed over the filling structure 212 and inner shaft 214, is retracted to expose the second filling structure 212 at the target treatment site.

In an exemplary method, first, the balloon 116 or 216 is expanded. Expanding the balloon 116 or 216 expands the corresponding filling structure 112 or 212 and endoframe 127, 227 disposed thereon. Next, the expanded filling structure 112 or 212 is filled with the fluid filling medium. Then, the balloon 116 or 216 is deflated to allow a flow of blood through the filling structure 112, 212 filled with the fluid filling medium, while the expanded endoframe 127, 227 maintains the patency of the generally tubular lumen within the expanded filled filling structure 112 or 212. In another embodiment, one or both of filling structures 112 or 212 are be filled with the fluid filling medium first, then the balloon 116 or 216 expanded to expand the endoframe 127 or 227 to form a generally tubular lumen in the corresponding filling structure 112 or 212. In still another embodiment, filling structure 112 or 212 is filled with the fluid filling medium simultaneously with expanding the balloon 116 or 216 disposed therein. Typical variations of deployment procedures may include: one of the filling structures 112, 212 and associated balloons 116, 216 being expanded first along with the corresponding endoframe 127, 227, followed by the other filling structure, endoframe and balloon. As discussed in the configurations described below, both balloons are radially expanded simultaneously thereby also expanding the filling structures and endoframes simultaneously.

Alternatively, one or both filling structures 112, 212 may be filled with a hardenable material and then the filling structures 112, 212 are radially expanded along with the corresponding endoframe 127, 227. In still other embodiments, combinations of filling and expanding may be performed in different order depending on physician preference and aneurysm anatomy. In some embodiments, an optional pre-filling step may be performed prior to filling with the hardenable filling medium. In this optional step, once the delivery system is positioned across the aneurysm, the filling structure may be filled with CO₂ gas, contrast media, saline or other fluids to unfurl the filling structure 12 away from the delivery catheter thereby helping to ensure more uniform filling later on and reduce or eliminate stiction between folds of the filling structure that may be present. During unfurling, the filling structure may be partially filled or fully filled so that it conforms to the inner aneurysm wall. Once unfurled, angiography may be performed through a fenestrated nosecone 133 or 233 on the inner catheters shafts 114 or 214 upstream of the aneurysm to detect leaks in the deployed filling structure 12. Once an optimal filling volume and pressure is determined to prevent the occurrence of endoleaks, the fluid may be removed from the filling structure and it may be filled with the hardenable material to expand and conform to the aneurysmal space between the lumens and the inner aneurysm wall. Pressure relief valves such as those described herein may also be used to ensure that the filling structure is not over filled. In order to prevent overfilling of the filling structure, any of the pressure relief valves disclosed below may also be used to bleed off excess fluid from the filling structure.

FIG. 10D illustrates the simultaneous inflation of both balloons 116, 216 along with endoframes 127, 227 in addition to expansion and filling of filling structures 112, 212. The filling structures and balloons are expanded and inflated to fill the aneurysmal volume in contact with the aneurysmal wall and each other, as illustrated in FIG. 10E. U.S. Patent Publication No. 2006/0212112 discloses filling of one filling structure in more detail including pressures, filling materials and other details, the entire contents of which have previously

17

been incorporated herein by reference. FIG. 10E also illustrates a cut away view of the expanded endoframes 127, 227 within the filled filling structures 112, 212. The upper ends of the balloons 116 and 216 will conform the tubular lumens of the filling structures against the walls of the aorta as well as against each other, while the lower ends of the balloons 116 and 216 will conform the tubular lumens into the respective iliac artery, IA. The expanded endoframe 127 not only provides support to filling structure 112, but also creates and shapes a lumen for blood passage from the aorta to one of the iliac arteries. Similarly, expanded endoframe 197 also provides a lumen for blood passage from the aorta into the other iliac artery. In some protocols filling of the filling structures (either both filled simultaneously or one after the other) may be performed before, during or after radial expansion of the balloons and the endoframe 127, 227 (either both expanded simultaneously or one after the other). Additionally, as discussed above with respect to FIG. 9, the endoframes 127, 227 may be radially expanded using a cylindrically shaped balloon to form a substantially cylindrically shaped lumen. Curved, tapered or pre-shaped balloons may also be used to expand the endoframes 127, 227, thereby forming a lumen that also is curved, tapered or shaped. The curved, tapered or pre-shaped balloon may be selected to match the anatomy of the vessel in which the endoframe and endograft is placed. Pre-shaped, curved or tapered balloons may be used in any of the other embodiments disclosed herein in order to obtain a desired lumen shape.

After filling the filling structures 112 and 212 as illustrated in FIG. 10E, the filling materials or medium will be cured or otherwise hardened as described in U.S. Patent Publication No. 2006/0212112 and the inner delivery catheter shafts 114 and 214 removed, respectively. The hardened filling structures along with the expanded endoframes 127, 227 will then provide a pair of tubular lumens opening from the aorta beneath the renal arteries to the right and left iliac arteries, as shown more clearly in broken line in FIG. 10F. The ability of the filling structures 112 and 212 to conform to the inner surface (S) of the aneurysm, as shown in FIG. 10F, helps the structures to remain immobilized within the aneurysm with little or no migration. Immobilization of the filling structures 112 and 212 may be further enhanced by providing any of the surface features described in U.S. Patent Publication No. 2006/0212112 which has been incorporated herein by reference.

The double filling structure embodiments may include at least one endoframe deployed within each of the tubular blood flow lumens. The endoframes will generally be endoskeletal structures that lay the foundation for new lumens, and will be deployed within the tubular lumens of the double-walled filling structures using balloon or other expansion catheters (in the case of malleable or balloon-expandable endoframes) and an optional retractable constraining sheath. FIG. 10G more clearly shows the first endoframe 127 disposed within the generally tubular lumen of the first filling structure 112 while a second endoframe 197 is disposed in the tubular lumen of the second filling structure 212. As illustrated, in this exemplary embodiment, the endoframes are balloon expandable structures which extend into the iliac arteries IA at the lower end of the filling structures. In other embodiments, the endoframes may be self-expanding endoframe-like structures fabricated from a shape memory alloy such as Nitinol.

Referring now to FIG. 10H, first and second endoframes 127 and 227 may extend upwardly on the aortic side of the first and second filling structures 112 and 212. In such embodiments, the first and second endoframes 127 and 227

18

may be constructed so as to not obstruct the renal arteries. For example, the first and second filling structure 112 and 212 may include a side hole so as to allow flow of blood through the renal arteries (RA). When the endoframe structures extend into the thoracic aorta TA, it will usually be desirable that they be expanded so that they conform to each other along a plane or region of contact. For example, as shown in FIG. 10I, the upper ends of the endoframes 127, 227 may be formed from their respective expansion balloons and manufacturing shape treatments to have D-shaped cross-sections when expanded, although other cross-sections such as elliptical, circular, etc. may be formed. Thus, flat faces 258 and 260 will engage each other with the remaining portion of the endoframe conforming to the inner wall of the aorta. In this way, most of the cross-sectional area of the aorta will be covered with the endoframe, thus enhancing blood flow through the filling structures. Other configurations are disclosed in U.S. Patent Publication No. 2006/0212112 previously incorporated herein by reference.

In the exemplary embodiment of FIGS. 10A-10I, each endoframe and filling structure is both disposed coaxially and generally concentrically over an expandable member coupled to a delivery catheter and the entire system is delivered to the aneurysm at one time. Such a coaxial and concentric system, such as that shown in FIG. 8, typically includes a filling structure 12, also referred to as an endograft that is coaxially disposed over the endoframe 19, both of which are then coaxially and concentrically positioned over a radially expandable balloon 16 which is coupled to the distal region of a inner shaft 17. Proximal and distal portions of endoframe 19 may extend uncovered by filling structure 12 and a filling tube 20 allows a fluid to be delivered to the filling structure 12. Under certain conditions, endoleaks occur, thereby resulting in incomplete occlusion of the aneurysm. Although a separate angiography catheter may be useful to visualize the blood flow through the aneurysm and detect endoleaks during deployment, a separate angiography catheter would likely increase the profile and further complicate the method of delivery. Additionally, in certain situations, the filling structure may move relative to the endoframe during delivery, thereby resulting in inaccurate placement of one or both devices.

It would therefore be advantageous an integrated system provide a system that can perform an angiography procedure without substantially increasing the profile of the delivery system or over complicating the procedure. It would be further advantageous for such a system to provide more effective ways of coupling the filling structure and endoframe to the delivery catheter to inhibit movement and facilitate more accurate delivery of the endoframe and endograft to the treatment site.

FIGS. 11A-11B illustrate an exemplary embodiment of a delivery system having a fenestrated nosecone 33 and a retractable outer sheath 40, as shown both during delivery of the system to the aneurysm (FIG. 11A) and during deployment of the filling structure at the aneurysm (FIG. 11B). The exemplary embodiment includes an inner shaft 17 having a filling structure 12 and endoframe 19 disposed thereon, and an outer sheath 40 slidably disposed over the inner shaft 17, filling structure 12 and endoframe 19. Nosecone 33, attached to the distal end of inner shaft 17, includes a lumen extending therethrough, preferably a single through lumen, the through lumen connected to a guidewire lumen of the inner shaft 17, such that the nosecone and inner shaft can be simultaneously advanced along the same guidewire GW. The nosecone includes a series of sideports 34 in fluid communication with the through lumen for performing angiography before, during

19

or after deployment of the filling structure 12. The system includes releasable coupling mechanisms to attach filling 10 and endoframe 19 to inner delivery catheter 17 during delivery of the system to the aneurysm (shown in detail in FIGS. 20A-20E). The distal end of outer sheath 40 releasably couples with the nosecone to facilitate advancement of the system through a patient's vasculature, as illustrated in FIG. 11A. A marker band 31 may be disposed near the interface on one or both of the proximal portion of nosecone 33 and the distal end of the outer sheath 40, so as to allow a user to visualize the location of the outer sheath 40 relative to the filling structure 12. Once the filling structure is positioned as desired, outer sheath 40 can be retracted relative to the filling structure 12 and inner shaft 17, as shown in FIG. 11B, thereby exposing the filling structure for deployment within the aneurysm. The fenestrated nosecone remains attached to the end of the inner shaft 17 distal of the filling structure 12 so that an angiography procedure may be performed. For example, as shown in FIG. 11B, a contrast media 38 may be injected through the guidewire lumen of the inner shaft 17 and out through the side ports 34 of the nosecone 33 into the vasculature. In one embodiment, outer sheath 40 is retracted by pulling proximally on an annular knob 57 depicted in FIG. 15. After deployment and release of the filling structure and endoframe from the inner catheter, outer sheath 40 can be advanced, typically using knob 57, so as to interface with nosecone 33 to facilitate withdrawal of the system from the patient.

FIG. 12 shows an exemplary embodiment of the delivery system, which includes the fenestrated nosecone 33, an outer sheath 40, a filling structure 12 (not shown) disposed within outer sheath 40, an annular carrier knob 57 for retracting the outer sheath 40, and a handle 60. In an exemplary method of treating an aneurysm, the system, as shown in FIG. 12, is inserted into the vasculature of the patient. The distal tapered shape of nosecone 33 and the smooth transition between the nosecone 33 and outer sheath 40 coupled thereto facilitates advancement of the system through the vasculature of the patient. Once the filling structure 12 is positioned at the aneurysm treatment site, the physician may retract the outer sheath 40 by pulling carrier knob 57 proximally, thereby retracting outer sheath 40 over hypotube 41 proximal of knob 57. The carrier knob 57 is fixedly attached to the proximal end of outer sheath 40 and includes a seal between outer sheath 40 and hypotube 41. Handle 60, disposed at the proximal end of inner shaft 17 is used to advance and withdraw the system, as well as to deploy the (fillable) filling structure 12 or perform angiography through nosecone 33.

Fenestrated Nosecone

FIG. 13 illustrates the nosecone 33 of the embodiment of FIG. 12 in more detail. Although shown in the embodiment of FIG. 12, nosecone 33 may be incorporated into any of the embodiments disclosed herein. Nosecone 33 is distally tapered and includes a through lumen 18 extending along a longitudinal axis of the nosecone to facilitate advancement of the system over a guidewire through the vasculature. Nosecone 33 is also fenestrated having a series of sideports in fluid communication with the through lumen for performing angiography. The through lumen 18 of the nosecone is sized so as to simultaneously receive a guidewire and a flow of contrast media for performing angiography through the side ports 34. The fenestrated nosecone 33 is advantageous as it facilitates both advancement of the system over a guidewire and delivery of contrast media in an angiography procedure through the same lumen while the guidewire is disposed therein, thereby simplifying the procedure while maintaining a reduce profile.

20

To facilitate both advancement of the system and deployment of the filling structure, fenestrated nosecone 33 releasably couples or interfaces with the distal end of outer sheath 40. In an exemplary embodiment, nosecone 33 includes an isodiametric portion 36 which is isodiametric with the outer diameter of the distal end of outer sheath 40 so as to create a smooth transition at the interface and prevent "snowplowing" against a vessel wall as the system advances through the patient's vasculature. Isodiametric portion 36 extends a distance distal of the interface so as to increase the stiffness of the nosecone near the interface and prevent flexure of the nosecone and/or outer sheath at the interface during advancement of the system. Nosecone 33 may also include a portion 37 having an outside diameter slightly smaller than the inside diameter of the distal end of outer sheath 40; thus, portion 37 is disposed within the outer sheath 40 such that the outer sheath 40 fittingly receives portion 37 so as to releasably couple with the nosecone 33. Portion 37 may extend a distance proximal of the interface so as to increase the stability of the coupling and to increase the stiffness near the interface to prevent separation between the nosecone and outer sheath 40 as the system winds through complex or tortuous vasculature, thereby further reinforcing the smooth transition between the nosecone 33 and the outer sheath 40 to reduce the likelihood of "snowplowing" against the vessel wall. The nosecone 33 and/or the outer sheath 40 may further include a radiopaque marker band 31 near the interface to allow a physician to image the location of the distal end of the outer sheath 40 relative to nosecone 33. The resin to manufacture the nosecone may also include a radiopaque filler to facilitate imaging during the procedure.

Nosecone 33 is dimensioned to facilitate advancement in a patient's vasculature. An exemplary nosecone may be between 1 to 4 inches in length, preferably 2.5 to 3 inches, and have an outside diameter tapering from about 0.25 inches at a proximal end to about 0.050 inches at a distal end. The through lumen 18 extending through the nosecone 33 may also reduce in size as the outside diameter tapers down. For example, the through lumen at the proximal end 32B may be between 0.05 and 0.1 inches, preferably about 0.08 inches, and reduce in size gradually or incrementally to 0.02 to 0.04 inches, preferably about 0.05 inches at the distal portion 32A of nosecone 33.

Angiography may be performed by injecting a contrast media through the guidewire lumen of the inner shaft 17, which then flow into the through lumen 18 of nosecone 33 and out the side ports 34, preferably while the guidewire GW is disposed within the guidewire lumen and through lumen 18. Angiography may be performed through nosecone 33 before, during, or after treatment of the aneurysm, and is useful for imaging the flow of blood, particularly for detecting leaks in an endograft deployed in an aneurysm. In an angiography procedure, a radiopaque contrast media is delivered into a blood vessel and an X-ray based imaging technique, such as fluoroscopy, is used to image the flow of the contrast media as it flows through the blood vessel. Thus, the contrast media is released uniformly into the blood vessel so that the imaging produces a more accurate representation of blood flow through the vessel.

In an many embodiments, fenestrated nosecone 33 includes pairs of side ports 34 arranged in a series equally distributed along the nosecone in a helical fashion so as to evenly distribute the contrast media into the vasculature. Preferably, each of side ports 34 extends in an orthogonal direction from the longitudinal axis of the nosecone 33. In an exemplary embodiment, the nosecone 33 comprises a series of 4 to 10 pairs of side ports 34, preferably 5 to 7 pairs of side

21

ports, arranged in a helical fashion as described above. Typically, a side port **34** has a diameter within a range of 0.01 inches to 0.05 inches, and more preferably within a range of 0.03 to 0.04 inches.

FIG. **14** illustrates the nosecone **33** having a guidewire GW disposed within guidewire lumen **18** as well as a flow of contrast media **38** through a portion of guidewire lumen **18**. In an exemplary embodiment, the guidewire lumen **18** includes a distal portion **32A** which is reduced in size from the guidewire lumen **18** at the proximal end of nosecone **33**. Distal portion **32A** of the through lumen **18** is sized to slidably receive the guidewire and fit so as to inhibit flow of contrast media through the distal opening when the guidewire is disposed therein. The portion of the through lumen **18** proximal of portion **32A**, however, is sized to simultaneously receive the guidewire and facilitate flow of contrast media **38**. The narrowed distal region **32A** of through lumen **18** substantially inhibits flow of contrast media through the distal opening of the nosecone, thereby directing the flow of contrast media through the side ports **34** and into the vasculature of the patient, as illustrated in FIG. **14**.

Annular Knob

FIG. **15** illustrates the carrier knob of the system of FIG. **12**, the carrier knob coupling the proximal end of outer sheath **40** with hypotube **41**. In such an embodiment, the outer sheath **40** is slidably disposed, at least partially, over hypotube **41** (main catheter shaft) when outer sheath **40** is retracted. In use, outer sheath **40** is retracted relative to the inner shaft **17** to expose the filling structure **12**, endoframe **19** and expandable member, i.e., balloon **16**, on a distal region of inner shaft **17**. The carrier knob **57** is fixedly coupled to the proximal end of the outer sheath **40**, preferably with a heat bond, so that a physician may manually pull the carrier knob **57** to retract outer sheath **40** over hypotube **41**. Carrier knob **57** may also include an internal seal. The carrier knob **57** may comprise any material, such as polyetheramide, which can be bonded with the outer sheath **40**.

Carrier knob **57** may include an internal seal **56**, such as an silicone O-ring, to prevent fluid outflow from between the distal and proximal segments of the outer sheath **40**. Typically, the blood pressure of the patient against internal seal **56** is sufficient to prevent fluid outflow from the body between outer sheath **40** and hypotube **41**. As the carrier knob **57** is pulled proximally internal seal **56** slides proximally contacting the outer surface of the hypotube **41** and inside the annular knob **57**.

Carrier knob **57** may be heat bonded to the outer sheath **40** by covering the proximal end of outer sheath **40** by a laminate material, preferably a polymer material such as Pebax®, placing a cavity in the knob **57** over the laminate covered outer sheath **40**, and heating the assembly so that the laminate bonds to the outer shaft **40** and/or the knob **57**, preferably bonding with both the outside surface of outer sheath **40** and the inside surface of the knob **57**. The system may further include a retaining mechanism to prevent the hypotube **41** from slipping out of the knob **57** when the outer sheath **40** is advanced. The retaining mechanism may comprise a collar, a ring, a pin, a screw or any mechanism suitable to maintain a slidable coupling between the hypotube **41** and the annular knob **57**. The system may also include a keying mechanism to prevent rotation between hypotube **41** (main catheter shaft) and sheath **40**. Knob **57** include a sheath flush line **63**, to allows flushing of the sheath or shooting contract through the sheath during the treatment procedure.

Handle

FIG. **16** illustrates a handle **60** of an exemplary delivery system of FIG. **12**. Handle **60** include a body having a

22

guidewire access port **61**, an angiography line **62**, a fill tube line **64**, a release wire port/connector **66**, and a balloon inflation line **68**. The angiography line **62** provides access to the guidewire lumen such that contrast media can be injected through the guidewire lumen and out the series of side ports **34** of the nosecone **33**. As the contrast media may be viscous, the backend pressure needed to perform angiography may reach 1,000 psi or more.

These pressures may potentially cause the guidewire to “shoot” out of the guidewire lumen. To prevent this from happening, the guidewire access port **61** may include a locking mechanism for locking guidewire GW to the handle during the angiography process. Thus, angiography line **62** provides access to the guidewire lumen, while the guidewire access **61** may seal and lock the guidewire GW into place. Release wire access port/connector **66** provides access for removal of the release wire so as to decouple the coupling mechanisms and release the deployed filling structure from the inner shaft **17**. Release wire access port/connector **66** may include a threaded luer type connector, which is fixed to the proximal end of the release wire, such that removing the port connector (along with the filling structure fill tube **64**) and pulling in the proximal direction will retract the release wire and decouple the coupling mechanisms. Optionally, handle **60** may rotate on its inner and outer shafts to prevent undesired transfer of torque to the catheter shafts. The descriptions of additional components depicted are included in the descriptions of FIGS. **18** and **21**.

A pressure monitor **69** is utilized to monitor the filling structure filling pressure during the treatment procedure. Typically, the pressure monitor is fluidly coupled with the filling tube circuit so as to monitor the system filling pressure during filling of the filling structure **12** with the hardenable medium.

Pressure Monitoring

In an exemplary method of simultaneous action in deploying filling structures and endoframes in separate catheters, pressure monitoring may be utilized in the following way.

After two filling structures have been delivered to the treatment site, both endoframes are radially expanded to help create a lumen for blood flow through the filling structure across the aneurysm. Using data from a patient’s computerized tomography (CT) scans, a fill volume of the aneurysm treatment site may be estimated. This represents the baseline filling volume for both filling structure and is the minimum expected volume of filling material to be injected into the filling structure feed circuitry. Syringes or other injection devices coupled with a pressure gage may be used to optionally pre-fill each filling structure with contrast material using the baseline volume and the resulting baseline fill pressure may be noted. In addition, the pressure monitoring system may include a pop-off valve to relieve excess pressure in the event of overfilling. The pressure monitoring system may include a sensor inside the filling structure and a sensor monitoring the patient’s systolic and or diastolic blood pressure used for calculating the patient’s differential blood pressure. A differential blood pressure reading between the filling structure and the patient’s systolic and or diastolic pressure simplifies the process of filling the structures as this allows the physician to accurately target the pressure inside the filling structure. This allows unfurling of the filling structure and provides a preliminary assessment of how the expanded filling structures fit into the aneurysmal space. Once this is accomplished, the contrast material is removed from the filling structures (in a method utilizing a pre-filling step). Again using the patient CT data, a functional fill volume may be determined. This volume is a percentage of the aneurysm

volume obtained from the CT data, or it may be a predetermined number and is the volume of filling material that effectively seals and excludes the aneurysm.

Functional fill pressure will be the pressure at which the functional fill volume is attained. A polymer fill dispenser may then be used to fill each filling structure with the functional fill volume and the functional fill pressure is noted. While holding the functional fill volume and pressure, the filling structure may be observed under fluoroscopy to check for proper positioning, filling and the absence of leakage across the aneurysm. If leaks are observed, additional polymer may be added to the filling structures until the leaks are prevented or minimized. Excessive additional polymer should not be added to the filling structure in order to avoid exceeding a safe fill volume or safe fill pressure. Once the physician is satisfied with the filling and positioning of the filling structures, stopcocks to the filling structures may be closed to allow the polymer to harden and then the delivery devices may be removed from the patient.

FIG. 17 illustrates a pressure monitor 69 comprising an integrated pressure gauge transducer. Pressure monitor 69 may include a body 70, a pressure fitting 71, control buttons 72, and a digital display 73 for reading the pressure and time output. The body 70 may include pressure transducers for determining the pressure and/or differential pressure. Pressure fitting 71 couples the pressure transducers of the body 70 to the filling system, control buttons 72 allow a user to adjust the pressure or the pressure or time readout. The pressure fitting 71 may include a tubular member and a luer cap for fluidly coupling with a filling line of the delivery system 10. Pressure monitor 69, or a portion thereof, may be re-usable or disposable, preferably the pressure transducers are for a single use and are disposable. In addition to actual pressure monitoring by gages and graphical displays etc., other pressure indicators may also be used to facilitate determining the filling status of the filling structure. For example, some embodiments may employ a relief valve. The relief valve is preset to a certain pressure such that beyond the preset pressure, any additional filling material will bleed out of the filling structure. While the relief valve may be adjacent the filling structure, preferably the filling material will be vented toward the proximal end (handle end) of the catheter, outside the body. This keeps potentially dangerous fluids or other filling material from being introduced into the body.

The methods may also include use of a pressure monitoring system that allows a physician to monitor the pressure before, during or after filling the filling structure. The system may include a user interface for displaying the pressure output and may optionally include a time output displayed in conjunction with the pressure output. The monitoring system may also include a processor for analyzing the pressure data. The processor may be programmed to normalize the pressure data. The pressure monitoring system enables the physician to closely monitor the filling pressure during deployment of the filling structure and may include additional functions to facilitate proper deployment, including: pressure cut-off switches, warning indicators if the measured filling pressure is outside an acceptable range, and pressure bleed off switches to optimize filling pressure and compensate for fluctuations in pressure during filling.

The monitoring system may also record the pressure data during deployment. Additionally, in embodiments deploying two filling structures, the monitoring systems may be operatively coupled such that the system or a physician may monitor pressures during filling of one filling structure in response to pressure output readings from the other adjacent filling structures.

Pressure monitoring can also be performed at various stages of the aneurysm repair procedure to help control the filling process of the filling structure. The monitoring of pressures serves to reduce the risk of dissection, rupture or damage to the aneurysm from over pressurization and also can be used to determine an endpoint for filling. Monitoring can be done before, during or after filling and hardening of the filling structure with filling medium. Specific pressures which can be monitored include the pressure within the internal space of the filling structure as well as the pressure in the space between the external walls of the filling structure and the inner wall of the aneurysm. A composite measurement can also be made combining pressures such as those measured within the interior space of the filling structure, together with that in the space between the external walls of the structure and the aneurysm wall or other space at the aneurysm site and an external delivery pressure used by a fluid delivery device, such as a pump or syringe, to deliver the filling medium. Control decisions can be made using any one of these pressure measurements or a combination thereof. Methods of pressure monitoring are discussed in detail in related commonly-owned applications: U.S. Pat. No. 7,666,220 and U.S. Patent Application No. US 20100036360 A1, the entire contents of which are incorporated herein by reference.

The pressure monitor as shown in FIG. 17 is used by an operator to monitor the filling pressure for the polymer being injected into the double wall filling structure 12. While a vacuum is initially pulled on the double wall filling structure 12, as described below, once the filling of the double wall filling structure 12 is initiated by the injection of polymer the associated pressure sensor monitor on the polymer tubing system as shown in FIG. 17 will detect the systemic blood pressure of the patient as the double walled filling structure 12 is surrounded by the patient's blood in the arterial system. As further injection of polymer progresses and any compressible fluid in the system becomes compressed (though there should be very little air or other compressible fluid in the system because a vacuum has been pulled on the system in the first step of the pressurization portion of the deployment procedure). The sensitivity of the pressure monitor to the blood pressure of the patient being treated will increase as more of the tubing system is filled with the liquid fluid (understood to be an incompressible fluid—which transmits pressure instantaneously). The system will then operate merely as a pressure sensor while the double walled filling structure 12 is unrestrained and surrounded by systemic blood pressurized in the normal manner by the patient's pulsating heart.

Pressure monitors 69, such as that shown in FIG. 17, can be programmed to display various desired systemic blood pressure specific points in the cycle of the pulsating blood pressure of a patient's normal arterial function. The high pressure being the systolic pressure and the low pressure in a cycle being the diastolic pressure. The pressure monitor, if so programmed, will provide a readout of both the systolic and diastolic pressures (two readings on one display face). The pressure monitor 69 can be reprogrammed (it's firmware adjusted) to readout specifically selected pressure parameters, e.g., the systolic pressure, the diastolic pressure, or a mean pressure (which averages the systolic pressure and diastolic pressure). The length of the sampling (averaging) time of the pressures measured and then displayed can also be adjusted in the pressure monitor 69. The averaging of each parameter over time can be taken over a selected range of seconds. For example the selected sampling ranges may be 5 seconds, 10 seconds, or 15 seconds, or other intervals desired—and available in the hardware and programmable software of the pressure monitoring device. The monitor will

25

then update its digital display at each selected time interval. In the normal operation of deployment of the filling structure, the operator will inject polymer into the double walled filling structure pressurization system and observe the diastolic pressure of the system. The diastolic pressure will vary according to system pressure (patients arterial blood pressure system pressure) until the outer wall of the double walled filling structure reaches the inner wall of the aneurysm. Simultaneously the inner wall of the double walled filling structure which is already adjacent to or situated on a support structure or endoframes (e.g., **19**) will become restricted in its inward expansion as a result of resting on against the internal support structure or endoframe. Once the limits of unopposed expansion are reached, the pressure inside the double walled filling structure (endobag) will increase. A monitoring of the pressure readout on the pressure monitor programmed to present either the diastolic pressure or the mean pressure will provide information about the state of expansion of the double walled filling structure. The polymer injection/filling should continue until the diastolic (lower) pressure is increased to be equal to or below above the systolic readout so that the mean pressure and diastolic pressure readout of the pressure monitor **69** is nearly the same (in the instance where all three pressures can be read on a display or detected by various means (known to person skilled in the art) during an operation. Once the endobag reaches its full expansion (limited from further expansion by the inner wall of the aneurysm), the pressure monitor **69** will no longer be measuring the system pressure or be sensing a variation system pressure. The diastolic pressure will not vary very much and the pressure in the double walled filling structure **12** (the endobag) will be shown on the digital display **73**. The target pressure for the endobag is usually at or slightly above the expected systolic pressure of the patient being treated. The pressure the systemic pressure expected to be overcome is in the range of 180 to 300 mmHg which is less than half an atmosphere (equal to 380 mmHg). Thus while the pressurization of the double walled filling structure initially reads the systemic arterial pressure, ultimately the arterial pressure is excluded and only the inner pressure of the double walled filling structure (endobag) is detected. Once the pressure inside the endobag exceeds the maximum systemic arterial pressure there is a high degree of reliability that the aneurysm is excluded and sealed. At that point further injection of the polymer will cease and possibly checking of the sealing by use of angiography can take place. There is a time duration of 5 to 10 min. from the initial injection time until the polymer becomes cured or set and during that 5 to 10 min. it may be possible to further inject polymer and detect the internal pressure of the double walled filling back **12**, if necessary. These aspects may be used in any of the methods and systems described herein.

FIG. **18** illustrates an exemplary delivery system and FIGS. **19A-19C** illustrate cross sections of the delivery system of FIG. **18**. FIG. **19A** shows cross-section A-A at a location proximal of the nosecone at which the filling structure **12**, endoframe **19** and balloon **16** are each disposed concentrically outside inner shaft **17** and inside of outer sheath **40**. FIG. **19B** shows cross-section B-B at a location distal of the carrier knob **57** at which concentric inner and outer filling tubes **20A**, **20B** are disposed adjacent concentric inner and outer balloon shafts **17A**, **17B** of inner shaft **17** within outer sheath **40**. FIG. **19C** shows cross-section C-C at a location between the handle **60** and carrier knob **57** at which concentric inner and outer filling tubes **20A**, **20B** are disposed adjacent concentric inner and outer balloon shafts **17A**, **17B** of inner shaft **17** within hypotube **41**. In many embodiments,

26

the outer sheath **40** and hypotube **41** comprise different materials. For example, the distal segment of outer sheath **40** may comprise polyether block amide, while the segment of outer sheath **40** proximal of the carrier knob **57** may comprise 304 stainless steel.

FIGS. **19B** and **19C** also show an inner core **99** or filler that typically terminates about 2.5 cm from the proximal (iliac side) balloon bond to the balloon outer shaft. The inner core **99** is typically a filler material, often a TPE material with a hardness of 70D (durometers on the D Shore scale) or lower (e.g. Pebax 6333). The inner core **99** can be a solid of a low durometer material, such as Pebax 6333, or a pellethane may be used so long as the density of the inner core aids in pushability. The outer surface of the inner core can be smooth or textured. Surface design of the inner core can be configured to provide a desired coefficient of friction low between it and the outer sheath. The distal end of the inner core **99** stops about 2 to 2.5 cm from the balloon taper/neck transition to allow for the balloon to expand and inhibit kinking of the fill tube. This transition is typically heat formed and UV bonded to create a tapered transition and to seal the lumens to ensure no air can pass through these lumens and inhibit back bleeding. At the handle end, the inner core can terminate 1 cm into the handle hypotube or can run entirely through the handle hypotube. Ideally, at least 1 cm of the inner core extends inside the handle hypotube to ensure attachment and inhibit kinking at this location.

Delivery System Coupling Mechanisms

FIGS. **20A-20E** illustrates coupling mechanisms of an exemplary delivery system. The coupling mechanisms inhibit movement of the filling structure and endoframe relative to the delivery catheter so as to facilitate positioning of the filling structure and endoframe at the aneurysm. FIG. **20A** depicts the coupling mechanisms during deployment of the filling structure, wherein the outer sheath **40** has been retracted and filling structure **12** has been partially filled. The coupling mechanisms may include tethers **51**, **53** and/or tether loops for attaching filling structure **12** and endoframe **19** to inner shaft **17**. As shown in FIG. **20A**, filling structure **12** is disposed over endoframe **19** which is crimped onto expandable member **16** disposed near the distal end of inner shaft **17**. Two releasable coupling mechanisms, tethers **51** and **53**, along with release wire **46** inhibit movement of filling structure **12** and endoframe **19** relative to inner shaft **17** during delivery and positioning at the aneurysm.

Tether **51** may comprise a tether loop fixedly attached to inner shaft **17** distal of the filling structure **12**, the tether loop extending through an opening in endoframe **19** and around release wire **46**, as shown in detail in FIG. **20E**. Tether **51** couples the endoframe **19** to inner shaft **17** so long as release wire **46** remains within the loop of tether **51**. In this embodiment, the filling structure **12** is indirectly coupled to inner shaft **17**, since endoframe **19** is also coupled to the filling structure **12** with sutures **47**. Once release wire **46** is withdrawn, tether loop **51** easily slips out through the opening in endoframe **19** and can be withdrawn with inner shaft **17**.

Tether **53** may comprise a tether loop fixedly attached to filling tube **20**, which then extends through a suture loop **45** on the proximal end of filling structure **12** and around the release wire **46**. So long as release wire **46** remains within the suture loop **45**, filling tube **20** remains coupled with the proximal end of filling structure **12**. Tether **53** may inhibit movement of the proximal region of the filling structure **12** during delivery, and may help prevent release of the fill tube **20** from the filling structure **12**. Thus, tether **53** provides a fail safe mechanism prior to filling and during filling or re-filling of the filling structure, until the procedure is over, at which time the release

27

wire can be retracted releasing the coupling between filling tube 20 and the filling structure 12.

Once the filling structure 12 has been deployed and filled with hardenable fluid filling medium, the release wire 46 can be withdrawn by pulling the proximal end of the release wire 46 from the handle 60. After releasing the filling structure 12 and endoframe 19, the delivery system 10) can be withdrawn from the body as tether loops 51 and 53 no longer couple the filling structure 12 or endoframe 19 to the system. In an exemplary embodiment, the release wire 46 extends the length of and runs parallel to inner shaft 17. During delivery, the distal end of release wire 46 is releasably coupled to inner shaft 17 just proximal of the nosecone 33, as shown in detail in FIG. 20D. This is to ensure the release wire does not interfere with deployment of the filling structure 12. A UV adhesive, such as Loctite 3321, may be applied to hold the knot and create a temporary bond between the release wire and the inner shaft. In many embodiments, release wire 46 is Teflon coated, so that the temporary bond easily delaminates and releases from inner shaft 17 when a physician pulls the proximal end of release wire 46 at handle 60. The release wire 46 may be made from polytetrafluoroethylene coated 304 stainless steel and sized so as to be easily withdrawn from between the filling structure 12 and the endoframe 19 after deployment.

As shown in FIG. 20B, filling structure 12 is coupled with the distal end of the endoframe 19 by one or more sutures 47, preferably four sutures, disposed at regular intervals about the distal end of filling structure 12. The sutures 47 couple the filling structure 12 to endoframe 19 to maintain the relative position of the endoframe 19 during deployment and may also help anchor the filling structure 12 to the endoframe 19 after deployment of the filling structure 12 in the aneurysm. One of skill in the art will appreciate that other releasable coupling mechanisms, including releasable knots, may be used and therefore the coupling mechanism is not limited to tether embodiments. Additionally, the tether may be used as a releasable coupling mechanism in any of the embodiments disclosed in this specification.

In an exemplary embodiment, suture 47 comprises a single thread having one end attached to endoframe 19 and the other end attached to endoframe 19, as shown in FIG. 20A. Alternatively, suture 47 may comprise a suture loop, such as those depicted in FIG. 20B. Endoframe 19 may include eyelets 49 near the proximal or distal ends of the endoframe through which the suture 47 can be looped to secure the filling structure 12 to the endoframe 19. This way, the filling structure 12 will be fixed relative to the endoframe as long as the tether loops are taut. Generally, this coupling mechanism will allow about ± 5 mm and more preferably ± 3 mm of relative movement between the filling structure and the endoframe. Also, the filling structure and endoframe should be positionable within ± 7 mm and more preferably between ± 5 mm of a target position within the aneurysm of the filling structure 12. In an exemplary embodiment, the four sutures are equally distributed about the distal end of the filling structure. For example, the four sutures may be attached to the filling structure and spaced apart radially at 0 degrees, 90 degrees, 180 degrees and 270 degrees.

FIG. 21 shows an undeployed configuration of delivery catheter 14A which includes an end handle 60A and a sheath retraction knob 57A. Sheath 40A is coupled to the sheath retraction knob 57A and is configured spaced apart from the end handle 60A by a hypotube 41A. The handle 60A includes a guidewire access port 61A through which a guidewire GW is passed. Next to the guidewire access port 61A there is a release wire access and lock port and fitting 66A through

28

which endobag pressurization piping (double wall filling structure 12) passes. One half of a quick release color-coded tubing connector 82A is connected to the catheter end of the endobag pressurization piping/tubing. Endoframe pressurization piping/tubing 68A (such as for balloon expansion within the endoframe) also passes into the handle 60A and has its catheter end connected to one half of a quick release tubing connector 84A. The handle 60A also provides routing for guidewire lumen pressurization piping/tubing 62A from one half of a quick release connector 86A at the catheter end of the tubing, to and through a tee fitting and external connection valve 75A through the tubing 62A into the handle and to the guidewire lumen connected therein. This guidewire lumen pressurization (angiography) tubing 62A and in line tee valve allow simultaneous introduction of contrast solution to both catheters or separate introduction of contrast solution to each catheter.

FIG. 22 shows the catheter 14A configured with its sheath 40A having been retracted over hypotube 41A by retracting the sheath retraction knob 57A towards the handle 60A such that the double walled filling structure 12A is exposed.

FIG. 23 shows a lateral view of two separate catheters 14A and 14B configured as they would be for deployment in separate legs of a patient routed through the patient's iliac arteries up into the patient's aorta. Each catheter 14A, 14B has the tubing of its respective handles 60A, 60B connected separately to a single operator sequential manifold console 300. The single operator manifold console 300 provides an operator the convenience, time savings benefit, and deployment operation self equalizing positioning of hooking both catheters 60A, 60B up to a single pressure port to use each step of an orchestrated series of steps to centrally, simultaneously, and equally pressurize the lumens and active elements of both separate catheter systems 14A, 14B. As shown in FIG. 23, the catheter handles 60A, 60B are configured symmetrically about the manifold console 300 to be connected with their corresponding common pressure and fluid supply lines from the manifold console 300. The handle 60A of catheter 14A includes, as previously discussed, a guidewire access port 61A while the catheter 14B and its handle 60B include a guidewire access port 61B. For the catheters pictured, similar structures on catheter 14A are similarly correspondingly numbered on catheter 14B except that the "A" suffix designation with respect to the elements of catheter 14A are transformed into "B" suffix designations when identified on catheter 14B.

The single operator manifold console has piping/tubing pressure and fluid supply lines leading to each to each corresponding fluid and pressure supply line function on the respective separate catheters. One half of quick release connection fittings at the ends of the tubing lines leading from the single operator manifold console are designated 83A for the endobag pressurization piping; 85A for the endoframe pressurization piping, and 87A for the guidewire lumen pressurization piping. The respective tubing leading from the single operator sequential manifold console 300 is designated 382A, 384A, and 386A. While on the second catheter 14B, the handle 60B houses similarly functioning fluid and pressure piping/tubing and quick connectors having a second set of pressurization lines leading from the single operator manifold console to the respective functioning pressurization lines of the catheter. The endobag pressurization piping 64B is connected to the manifold console tubing 382B through quick connector quick tubing connector halves 82B, 83B while the endoframe pressurization tubing 68B is connected to single operator manifold console tubing 384B through connector halves 84B, 85B and the guidewire lumen pressurization

29

pipings 62B is connected to single operator manifold console tubing 386B through quick connector halves 86B, 87B. On the catheter side of the manifold console there are six separate tubing lines leaving the console outlet opening 302. On the operator side of the manifold console 300 there are four tubing inlet lines: for endobag deflation (negative pressurization) 310, for endoframe pressurization (expansion of balloon) 320, for endobag polymer filling (positive pressurization) 330, and guidewire lumen pressurization (angiography (contrast) supply) 340.

Referring now to FIG. 24 which shows a plan view of the single operator sequential manifold console 300 four lines leading into the operator manifold console and six lines leading out of the console. However, the configuration with only three inlet lines may be used in other applicable systems where different sequential steps are desired/defined as recommended for deployment of the treatment structures associated with two separate catheters.

Although various configurations may be used, typically, a sequential configuration, such as first, second, and third ports for example, is arranged to match a recommended sequence of an operator's steps of operation such as pressure application to: endobag pressurization tubing, endoframe pressurization tubing, and guidewire lumen pressurization tubing. Functionally, there are only three separate (function) pressurization lines from each separate catheter connected to the sequential manifold console. Therefore a most simplified hypothetical manifold configuration would have only three lines matching the three separate system (functions) pressurization lines in the catheters. A console configuration for a catheter system utilizing three sequential steps of pressure application would be configured progressively (side by side) with three inlet ports to match the sequential steps of a deployment procedure requiring the operator to act (apply pressure) at a first inlet port, conclude activity at the first inlet port, act at a second inlet port, conclude activity at the second inlet port, act as a third inlet port, and conclude activity at the third inlet port in a sequential stepwise fashion. However, when two pressurization (positive or negative) activities need to be performed at one inlet port non-sequentially, (e.g., another step needs to be performed between the two (or more) steps to be performed at the one inlet port) the re-application or the attachment of a pressurization source and the re-application of pressure provide a non-ideal configuration in that the complexity of executing the recommended appointment steps shifts to the operator, and the operator must be knowledgeable and familiar with the deployment procedure to recognize and act on the three ports of the console while performing four or more steps of a deployment procedure. In this instance where only three steps are to be performed on the three inlet ports sequentially, a configuration of a manifold console as shown, would provide the benefit of simultaneous pressurization of the two separate catheters and their internal separate pressurization systems each from one pressure source as described herein for the configuration of FIG. 23.

The first inlet port into the manifold console 300 on the left side as shown in FIG. 24 is the endobag vacuum function with tubing 310 having a connection fitting 312 supplying the port. A sequence indicating symbol such as a number or letter is aligned with the first and subsequent adjacent inlet ports of the console. For port one here, the sequence indicating symbol 311 is the

Arabic number "one" adjacent to port one on the console. In addition, the word ENDOBAG may be listed in alignment with the first port on the face of the console. Port one also has an on-off switch/shutoff valve 314 aligned with it which can be used as a shutoff valve to close the tubing and prevent any

30

flow to or from port one. For example when vacuum is applied to port one, and there is no indication of blood in the endobag pressurization tubing, which would mean that there is a hole in the endobag and blood is being sucked into the tubing by the application of vacuum and that a vacuum pressure attained is maintained, the valve 314 can be closed to secure the system and release the vacuum source from the vacuum tubing connector 312.

A second port leading into the operator manifold console is associated endoframe pressurization tubing 320. The port associated sequence indicating symbol 321 is the Arabic number "two" on the console. The endoframe pressurization tubing 320 has a connection fitting 322 at its end.

The third port to the manifold console 300 adjacent to and to the right of the endoframe pressurization port in relation to the endoframes inlet tubing 320, endobag pressurization (polymer feed) tubing 330 has an end connection fitting 332 to which Tee and valve combination fitting 333 is connected. The side Tee fitting connection 334 is available for and is commonly used to monitor pressure by using a pressure monitoring device such as that shown and described in and for FIG. 17. The Tee and valve combination fitting 333 includes an inlet port 335 where a filler material (such as a hardenable fluid polymer) would be attached. The use of a valve fitting provides the ability to close the inlet port to isolate the endobag pressurization system when a supply source for polymer or other filling substance is replenished or replaced at the inlet port 335. The third port designator is labeled with Arabic numeral "three." A polymer cure visual indicator window 304 in the top of the console aligned with the third port provide visual indication of the completion of the curing process for a time curing polymer or filling material. Tubing, piping, or other conduit material having light transparent, translucent, or light transmissive properties is routed between a colored surface 330A and the indicator window 304. Polymer cure completion is detectable by a user when using a polymer or other filling substance which allows the colored surface 330A to be seen through the uncured polymer and tubing when the polymer is uncured, and then partially or fully obscures light passing through to prevent observing the colored surface through the polymer when the polymer is cured, as indicated by observing the obstruction of light and/or the loss of light transmissivity through the indicator.

The fourth inlet line to the manifold console 300 adjacent to and to the right of the third port in sequence, the guidewire lumen pressurization port being having inlet tubing 340 aligned with an alphanumeric designator 341 which in this instance is the Arabic number "four," 341. A guidewire lumen pressurization inlet port connector 342 is at the end of the tubing 340. A guidewire lumen pressurization port control on-off valve 344 is shown in line with the port. Such a valve prevent back leakage from blood being pressurized and finding its way through the guidewire lumen if left unchecked or may be used for angiography as described herein.

On the discharge side of the manifold console 300 the outlet opening 302 has six lines of tubing exiting. Two set of three lines of tubing are bundled by bracket connectors 380. The two bundles of lines each go to one catheter as previously discussed for FIGS. 22 and 23. The halves of the quick connect fittings at the ends of the tubing are configured to mate with complementarily matched halves of quick connect fittings on the catheters.

FIG. 25 shows an overview of all of the tubing/piping routed through the manifold console where the manifold console housing has been removed to reveal the routing of the tubing/piping. There are the four previously discussed supply lines 310, 320, 330, and 340 and the six console outlet tubing

31

lines 382A, 384A, 386A, 386B, 384B and 382B. The endobag vacuum connection line/tubing/piping/system is connected through on off switch/valve 314 which isolates the endobag inlet port connector 312 from the remainder of the tubing piping system. The guidewire lumen pressure supply tubing 340 is connected through the on off switch/valve 344 which isolates the angiography supply tubing which is fed into the guide wire lumens of the treatment catheters 14A, 14B. The polymer supply tubing line 330 is aligned with a polymer cure indicator window. The colored surface visual polymer siding indicator 330A reduces or eliminates the need to monitor the injection mixing and setting time for curing a polymer by providing a visual indication of successful conclusion of the treatment procedure.

FIG. 26 shows the vacuum connector (endobag pressurization) circuitry isolated from the other piping in the manifold console 300. A vacuum source is connected to the vacuum connector 312 thereby creating a vacuum pressure in connector line 310 sucks through the on off switch/valve 314 to reach a T connector fitting 315. The vacuum then reaches through the polymer cure indicator passage and the polymer cure indicator 330A to reach the downstream piping T connector fitting 316. The vacuum pressure is thereby distributed to the two treatment catheters through the endobag pressurization lines 382A, 382B. The quick disconnect fitting halves 83A, 83B connect to their complementary fitting halves on their respective endobag pressurization lines of the catheters. Once the endobag has been released from the sheath by retracting the sheath using the knob 57, a vacuum is pulled in the endobag piping, as the first step in the pressurization procedure to be sure that bag has no holes and its integrity is intact. Pulling a vacuum on the endobag cause any holes in the endobag to allow blood to the interior of the bag and to be sucked back through the tubing and towards the single operator manifold console. Since clear Tygon® tubing is used, the discoloration associated with a blood re-flow would be immediately apparent. Also if the tubing fails to maintain a vacuum, that would be an indication of some leakage or defect that would need to be explored further, even if blood was not immediately apparent in the tubing. Since this same tubing circuit would later be used and pressurized using the bag filling substance such as a polymer, the leakage of such filling substances from the piping system would be likely to occur at the location where a vacuum seal was not achieved during evacuation. Such leakage, while not universally catastrophic, may cause procedural delays and irregularities which might better be dealt with before the mixing and injection of pressurized expensive polymer into unknown locations by leakage from the piping system. Once the operator is satisfied that the endobags are in fact intact and sealed, the on off switch/valve 314 can be closed to isolate the endobags and maintain the vacuum while shutting off or disconnecting the vacuum source from the system and connector 312.

FIG. 27 shows an isolated view of the endoframe (balloon inflation) pressurization tubing/piping system used to expand endoframes as may be used in a treatment procedure. A pressurized fluid source is connected to the endoframe pressurization port 322 to provide fluid flow and pressure through: inflation tubing 320, a Y fitting 324, and branched into manifold console discharge tubing 384A and 384B, to reach their respective separate catheters as connected to and through their respective halves quick connect tubing/piping fittings 85A and 85B. Since the catheters inside the body are adjacent to one another spanning the aneurysm and the endoframes surrounding inflation balloons are adjacent to one another, simultaneous pressurization will equally distribute the pressure expanding the endoframes. Ideally the endoframes are

32

expanded such that they do not distort or distend the surrounding artery wall and damage to it. Once the endoframes are fully expanded, the endoframe (balloon expanding) pressurizing fluid can be removed or aspirated allowing the balloon to collapse to allow blood to flow through the now unfilled lumen of the expanded endoframes or others support structure (when an endoframe is not used). In the instance where self-expanding endoframes are used, the tubing/piping fitting or port associated with endoframe expansion may be omitted as the retraction of the sheath, e. g., sheath 40, earlier described or other such mechanisms could be used to release the compressed frame and initiate self expansion from its compressed contracted configuration to its relaxed open (expanded) configuration.

FIG. 28 shows the polymer filling piping (endobag pressurization) configuration where a polymer supply source is connected to polymer supply fitting 335. Polymer flows through the

T valve combination fitting 333 through the supply tubing 330 to the T fitting 315, through the polymer cure indicator tubing 344, to the T fitting 316, from where the polymer is equally pressurized to be distributed into the aneurysmal sac filling structures of both treatment catheters through discharge tubing and 382A, 382B, and the quick connect halves 83A, 83B connected thereto and to corresponding fitting and tubing on the separates treatment catheters. The vacuum pressure which has been maintained in the piping system since the first pressurization step of the treatment process is aids in initial polymer flow until pressure is equalized in the system, then when pressurized, polymer flows freely at a rate according to the resistance that the flow encounters in passing through the feed tubes and into the endobags. Once the polymer has set the endobag pressurization the operator may turn the release wire access port 66 (such as shown in FIG. 16) on the handle of each catheter to unlock it from the respective handle 60 and pull the port 66, fill tube 64, and release wire 46 (which is locked/fixed to the port 66 to release the endobag from the catheter for subsequent catheter removal).

FIG. 29 shows the angiography/contrast supply tubing (guidewire lumen) pressurization piping. The connector fitting 342 supplies contrast flow through the inlet tube 340 and through on off switch/valve 344 to a Y fitting 346 from where it is distributed to the two treatment catheters through supply tubing 386A, 386B and quick connector halves 87A, 87B, similar to the earlier described connections as would be understood by persons skilled in the art and may be used for pressurization of the guidewire lumen and/or angiography using the guidewire lumen as described herein.

While the above is a description of the embodiments, various alternatives, modifications, and equivalents may be used. For example, although the manifold console is described throughout as a single operator sequential manifold that allows a single user to operate the systems described herein, one of skill in the art would appreciate that various manifold consoles would be within the spirit and scope of the invention as described herein. The various features of the embodiments disclosed herein may be combined or substituted with one another. Therefore, the above description should not be taken as limiting in scope of the invention which is defined by the appended claims.

What is claimed is:

1. A system for treating an aneurysm comprising: a first catheter and a second catheter each catheter having an endobag, the endobag comprising a double-walled filling structure with an aneurysm conforming outer wall and a blood transit lumen creating an inner wall sur-

33

rounding an endoframe releasably coupled to the catheter and covered in an unexpanded configuration by a retractable sheath,

wherein each of the first and second catheters includes an endobag pressurization piping having one end releasably coupled to the respective endobag and an inner lumen in communication with the inside of the respective endobag with the other end of the respective endobag pressurization piping extending within the sheath and in communication with an endobag pressurization tubing outside the respective catheter,

wherein each of the first and second catheters comprises balloon on which the respective endoframe is mounted so as to expand the endoframe when inflated, wherein each balloon is in communication with an endoframe pressurization tubing outside of the respective catheter; and

wherein each of the first and second catheters comprises a guidewire lumen, each guidewire lumen being in communication with a guidewire lumen pressurization tubing extending outside of the respective catheter;

a sequential manifold console having two endobag pressurization tubing outlet ports, two endoframe pressurization tubing outlet ports, and two guidewire lumen pressurization outlet ports wherein the two endobag pressurization tubing outlet ports are connectable to the corresponding ends of the endobag pressurization tubing of the endobags of the first and second catheters, wherein the two endoframe pressurization tubing outlet ports are connectable to the corresponding ends of the endoframe pressurization tubing of the first and second catheters, and wherein the two guidewire lumen pressurization outlet ports are connectable to the corresponding ends of the guidewire lumen pressurization tubing of the first and second catheters;

the manifold console further having sequential inlet ports, wherein a first inlet port communicates with said two endobag pressurization tubing outlet ports, wherein a second inlet port communicates with said two endoframe pressurization tubing outlet ports, and wherein a third inlet port communicates with said two guidewire lumen pressurization outlet ports, wherein when said endobag pressurization and endoframe pressurization tubing ends from said first and said second catheters are connected to said corresponding manifold console outlet ports, such that pressurization of the first inlet port equally pressurizes corresponding endobag pressurization tubing to both the first and second catheters simultaneously and pressurization of the second inlet port equally pressurizes corresponding endoframe pressurization tubing to both the first catheter and said second catheter simultaneously;

wherein the first, second, and third inlet ports are configured in a side by side sequential configuration to provide operator guidance and to retain balanced pressurization between the first and second catheters, where the sequential configuration of first, second, and third ports is arranged to match a desired sequence of an operator's steps of pressure application to said first and second catheter endobag pressurization, endoframe pressurization, and guidewire lumen pressurization tubings, and

wherein said sequential manifold console includes a polymer cured indicator comprising a colored surface facing a light transmissive section of an endobag pressurization piping of the sequential manifold along a polymer flow path of said piping between said first inlet port and said two endobag pressurization tubing outlet ports, such that

34

a color of said colored surface can be seen by the operator through said light transmissive section of said piping when said piping is empty or is pressurized to contain uncured polymer and that said color of said colored surface is at least partially obstructed by a change in light.

2. The system for treating an aneurysm as in claim 1, wherein said sequential manifold console includes a fourth inlet port, which is also in communication with said endobag pressurization piping in said manifold console, where said fourth port is not located adjacent said first inlet port.

3. The system for treating an aneurysm as in claim 2, wherein said sequential manifold console includes a fourth inlet port flow valve which when closed prevents flow between said endobag pressurization piping in said sequential manifold console and said fourth inlet port.

4. The system for treating an aneurysm as in claim 2, wherein said sequential manifold console includes a third inlet port flow valve which when closed prevents flow between a guidewire lumen pressurization piping in said sequential manifold console and said third inlet port.

5. A sequential manifold console comprising:
two endobag pressurization tubing outlet ports;
two endoframe pressurization tubing outlet ports; and
two guidewire lumen pressurization outlet ports, wherein at least one of said two ports are connectable to an end of corresponding pressurization tubing outside of each of a first catheter and a second catheter;

the manifold console further having sequential inlet ports, wherein a first inlet port communicates with said two endobag pressurization tubing outlet ports, wherein a second inlet port communicates with said two endoframe pressurization tubing outlet ports, and wherein a third inlet port communicates with said two guidewire lumen pressurization outlet ports, wherein said corresponding manifold console outlet ports are connectable to said corresponding pressurization tubing ends comprising corresponding endobag pressurization tubing, corresponding endoframe pressurization tubing and corresponding guidewire lumen pressurization tubing of said first and said second catheters,

wherein the manifold console is configured such that pressurization of the first inlet port equally pressurizes the corresponding endobag pressurization tubing to both the first catheter and the second catheter simultaneously and pressurization of the second inlet port equally pressurizes the corresponding endoframe pressurization tubing to both the first catheter and the second catheter simultaneously;

wherein the first, second, and third inlet ports are configured in a side by side sequential configuration to provide operator guidance and to retain balanced pressurization between the first and second catheters, where the sequential configuration of first, second, and third ports is arranged to match a desired sequence of an operator's steps of pressure application to the connectable first and second catheter endobag pressurization, endoframe pressurization, and guidewire lumen pressurization tubing, and

wherein said sequential manifold console includes a polymer cured indicator comprising a colored surface facing a light transmissive section of an endobag pressurization piping of the sequential manifold console along a polymer flow path of said piping between said first inlet port and said two endobag pressurization tubing outlet ports, such that a color of said colored surface can be seen through said light transmissive section of said piping

when said piping is empty or is pressurized to contain uncured polymer and that said color of said colored surface is at least partially obstructed by a change in light transmissivity of the polymer as it cures thereby providing a visual confirmation by the obstruction of viewing 5 of the colored surface to the operator of the state of cure of the polymer.

6. The sequential manifold console as in claim 5, wherein said sequential manifold console includes a fourth inlet port, which is also in communication with said endobag pressurization piping in said manifold console, where said fourth port is not located adjacent said first inlet port. 10

7. The sequential manifold console as in claim 6, wherein said sequential manifold console includes a fourth inlet port flow valve which when closed prevents flow between said 15 endobag pressurization piping in said sequential manifold console and said fourth inlet port.

8. The sequential manifold console as in claim 5, wherein said sequential manifold console includes a third inlet port flow valve which when closed prevents flow between said 20 guidewire lumen pressurization piping in said sequential manifold console and said third inlet port.

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